

Road No. 22-A, County System  
in HAMBDEN TWP.

90

FIELD BOOK

3071

PLEASE RETURN TO  
GEAUGA COUNTY ENGINEER  
COURT HOUSE  
CHARDON, O.  
PHONE 250-X

Brakeman Road - No. 22 - Sec. A

Align. - pg - 1-20

Monuments - pg - 21-23

X-Sections - pg - 31-46

Slope Stakes - pg - 49-77

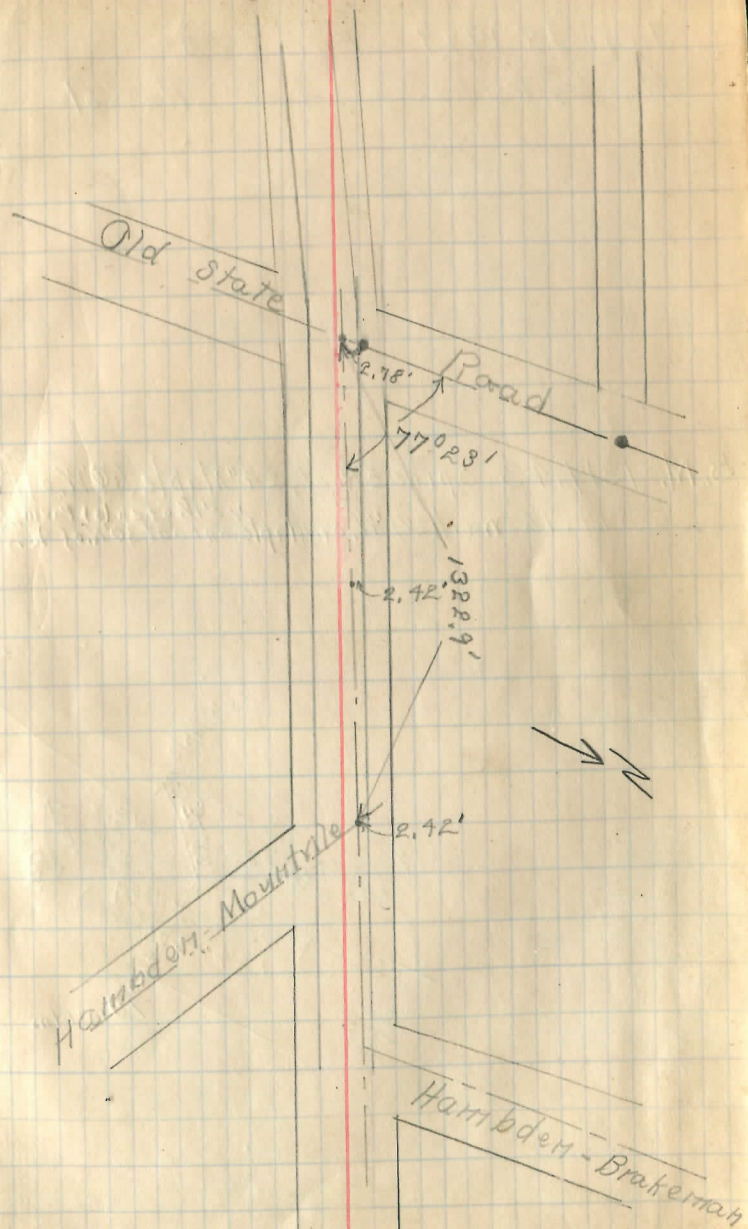
(90)

28.03

36 <sup>66</sup>

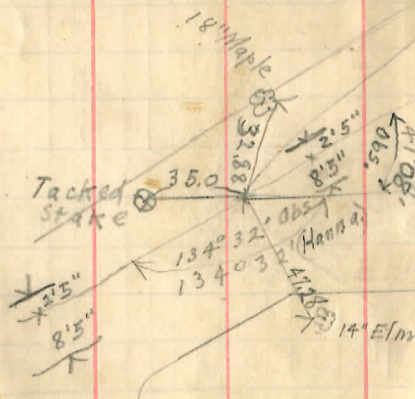
± 1433

± 1720

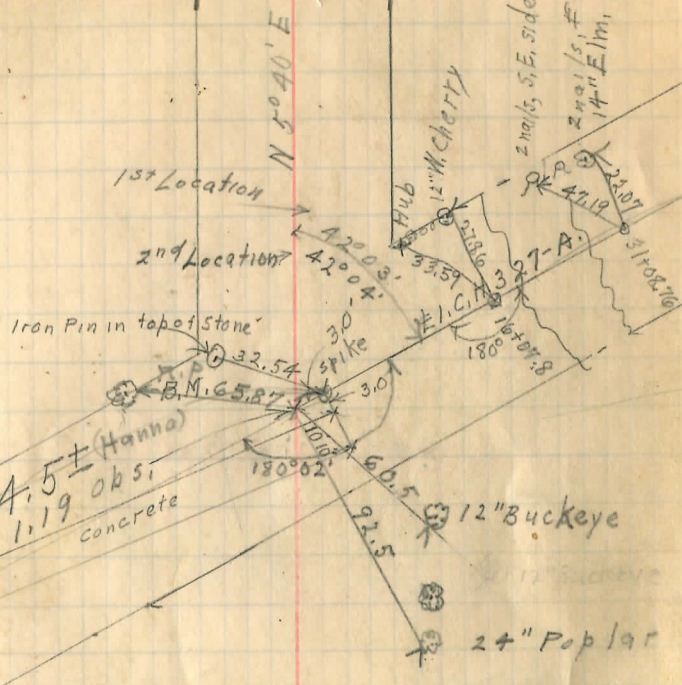


June 18, 1929 Fair 850  
 Marks, Parks, Goodrich, Hassel

B.M. 1319.43; Spike, E Root, 24" Maple, 60' W. of End  
 of Concrete  
 4' at the end of paving Conc.  
~~1319.16, north, 2 1/2' W. of Maple, on root 30' N. of E.~~



134.32  
 47.05  
 181.27



Hambden-Anclover Road I.C.H. 475

NOTE: SEE REF'S PAGE 21

3+47 T R3.5

x 4+00

< 22' x 03+68 Apples

x 3+00

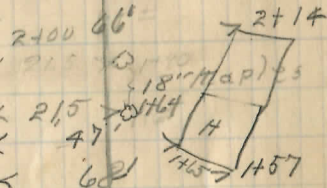
18" Maple

< 25' x 9+89

15" Buckeye

Stockham  
2+80

2nd Location  
1st Location



= 1+53

1+44 T < 2+1 x 3+9' x 1+44 18" Pine

< 22' x 1+35 18" Maple

< 30' x 1+21 18" pines

< 50' x 1+14

< 20' x 1+18  
1+08

x 1+00

x 2+1' x 0+92 gas Pump

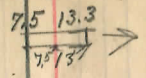
0+00 x 30' x spike

0+00

11+75.2

\* 3 X 2 stone Culvert, Fair as far as can be seen opening only 2" deep, needs cleaning, perhaps part new top. Extend with slab Top culvert, open outlet ditch 400'

\* 30" CMP EXISTING MAY 1987



11+56  $\swarrow$  21.5  $\searrow$   
11+21.5  $\times$  23'  $\times$  28'  $\times$  11+00 XH+02 15" Maple

9+69 FL. 10" Maple  $\swarrow$  29'  $\searrow$   
24" Elm  $\swarrow$  9+65  $\swarrow$  15'  $\searrow$   
9+53  $\swarrow$  25'  $\searrow$

2nd Location  
1st Location

7+83

7+52  $\swarrow$  24.5  $\searrow$  22.5  $\times$  7+41 8" Walnut

7+40  $\swarrow$  40  $\searrow$

7+30  $\swarrow$  30  $\searrow$  7+27  $\swarrow$  30  $\searrow$  7+21  $\swarrow$  30  $\searrow$

Weston 6+79 10" poor  $\swarrow$  65'  $\searrow$

6+78

Stockham

7" Maple  $\swarrow$  22.5  $\times$  6+30

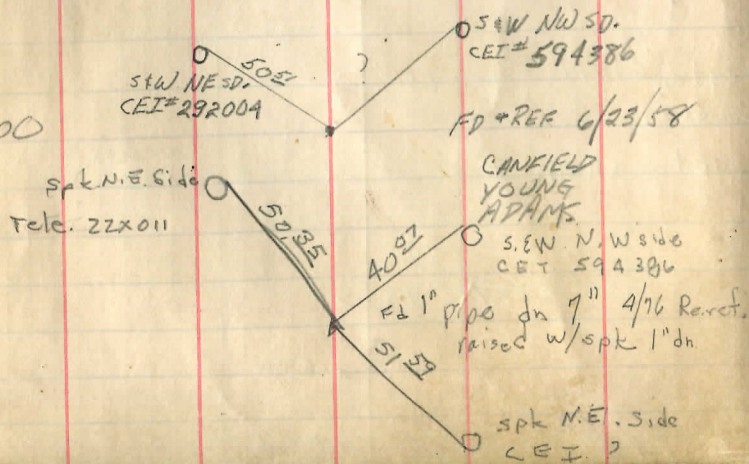
5+50  $\swarrow$  25.5  $\searrow$

x 5+00

15+00



15+00



June 19, 1929 S47 N07 D. Parks  
 850 P. Hassen  
 W. Goodrich  
 Stopped June 18<sup>th</sup> 1929

$\Delta = 0^{\circ}00'$

17170 w cherry  
 17+61  
 sycamore  
 17+31

16+94

16124  
 Hickory Nut  
 15+99  
 15+61

removed old pin  
 set new pin

13+55  
 P.L. ? 13+43

2<sup>nd</sup> Location  
 1<sup>st</sup> Location

35' 17+73 Maple  
 32' 17+32 Maple  
 35' 17+09 Maple  
 17+00  
 25' 16+96

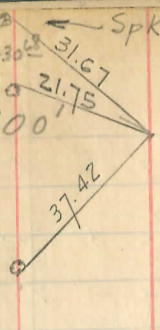
16110  
 23.0  
 21.0  
 900  
 30.0 Hub

12<sup>th</sup> Location  
 11<sup>th</sup> Location

22'  
 22'  
 22'

13+00  
 12+00

Spk N.E. side 15" Map. stump  
 S.W. side 192009  
 12" W. Ch  
 24+00  $\Delta = 0^{\circ}00'$



Spk S.E. side  
 14" Map

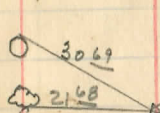
I.P. fd & reref.  
 6-22-42  
 P.m.  
 Wood.  
 Roofing nail set from  
 ref. 1-22-43 15/55

Fd. 4/23/58

D. CAMPBELL  
 T. ADAMS  
 R. YOONP

S.W. N.S. side  
 File 22X016

Spk S. Side  
 18" Cherry



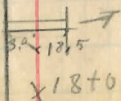
Spk N.W. side  
 14" Cherry  
 I.P. fd 4" dn 4/16/76 Reref

18+30.0 1x1 stone culvert, delapidated  
 Requires 24" Pipe

removed old pin  
 set new pin

23+66 X 13' >  
 23+47 X 24' >  
 22+98 X 24' >  
 22+71 X 24' >  
 22+10 X 22' >  
 8" Maple 21+90 X 23' >  
 RL 21+81 X X X >  
 21+63 X 20' >  
 W. cherry 21+58 X 20' >  
 21+00 X 21+00  
 10" Maple  
 20+61 X 28' >  
 15 Maple  
 20+33 X 28' >  
 20+00  
 19+91 X 21' >  
 8" W. cherry 19+76 X 21' >  
 19+75 X 21' >  
 19+62 X 21' >  
 19+00 X 19+00  
 18+00 X 18+00

2nd Location  
 1st Location





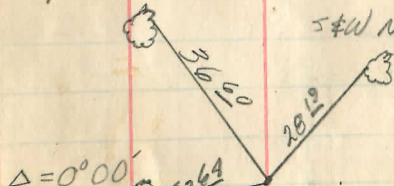






S&W NESD 12" MAR.

S&W NWSD 30" EIM



49750

$\Delta = 0^{\circ} 00'$

S&W 5th 20" MAR.

PIPE PL 5-55 3" down

REFER. 6/23/58

48+08

sheet iron corroded  
11" iron pipe

Require 12" Pipe

54155 X 31

54120 X 34.5

53787 < 21.5

51+25 < 21.0

P.L. 50140 X X X

50140

32

25'

50+11

50100

31

41'

18'

21

21.0

49100

48128 X 32.5

48109 X X X X

34.0

50+5.1

X 48+00

X 54+00

X 53+00

X 52+00

X 51+00

50+80

5'

50+64

50'

50+11

49791

4" EIM

24" Pear

49709

49749

4" EIM

4" EIM

4" EIM

H

460 49710

Maples

2nd Location  
1st Location

Ses

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

10

e1+11 Right, use 18" D.W. Pipe

~~57+95, location for 15" Hillside Culvert~~

62+68, P.L. <sup>1. P.</sup> 62+72 < 23 >

61+93 < 23 >

10124

59+93 < 21.5 >

57+90 < 21 >

55+87 < 22.5 >

< 39

< 21.5 >

x 62+00

< 22 >

< 31

< 39.5

< 31

x 29.5

< 27

x 60+00

x 59+60

x 58+00

< 25

x 57+00

< 25

x 56+00

< 6.8

x 55+00

Iron Pipe  
62+60

62+64 15" Cherry

62+00 Pine

61+92 10" Pine

61+71

H

61+31

61+23

10" Maple

20" 12" Vit. Pipe

61+11

60+98 12" Pear

60+87 10" Maple

P.L. 2

56+63

10" Cherry

56+49

55+83

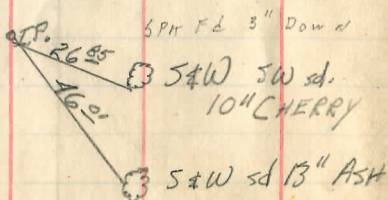
2<sup>nd</sup> Location  
1<sup>st</sup> Location

68+30

3 1/2' X 2 1/2' culvert, Stone Walls, repainted, good.  
~~3x3 concrete Box~~ New concrete slab,  
headwalls + Wing Walls. Extend  
Use as it is.

67+00

$\Delta = 0^{\circ}00'$



REF. 6/23/58  
D. CANFIELD  
T. ADAMS  
P. YOUNG

15" D.W.

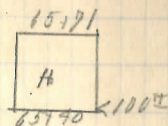
Pipe required 65102

Removed old pin

Set new pin 7.29

IPipe Fl

CRI. S+W SE SIDE



2nd Location

1st Location

8" Cherry  
63+93 of 37

X 71+00 X

X 70+00 X  
13.87

X 21.5 X 69.88 15" Cherry

X 21.5 X 69+70 15" Maple

X 21.5 X 69+50 15" Maple

X 69+00

P.L. 68+43

32

IRON PIPE

Corrected Line

10.8 19.8

X 68+00

X 155 X 67+98

67+56

X 31.5 X 27.5 X 67+56

X 67+00

X 66+00

X 12 X 65+98

X

X

X

X 65+00

X

X PIN

X PIN

X PIN

X PIN

X 64+25 PL

X 22 X 64+25 2 1/2" PINE GONE

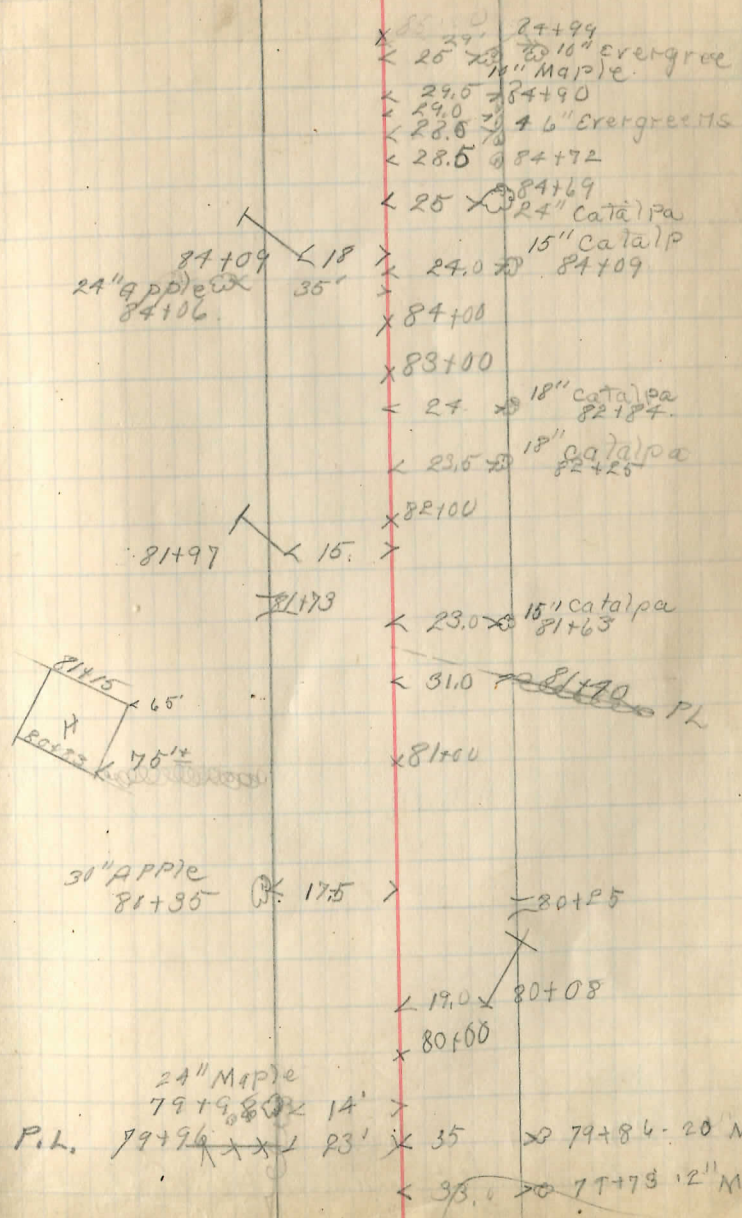
X 64+00

X 63+95

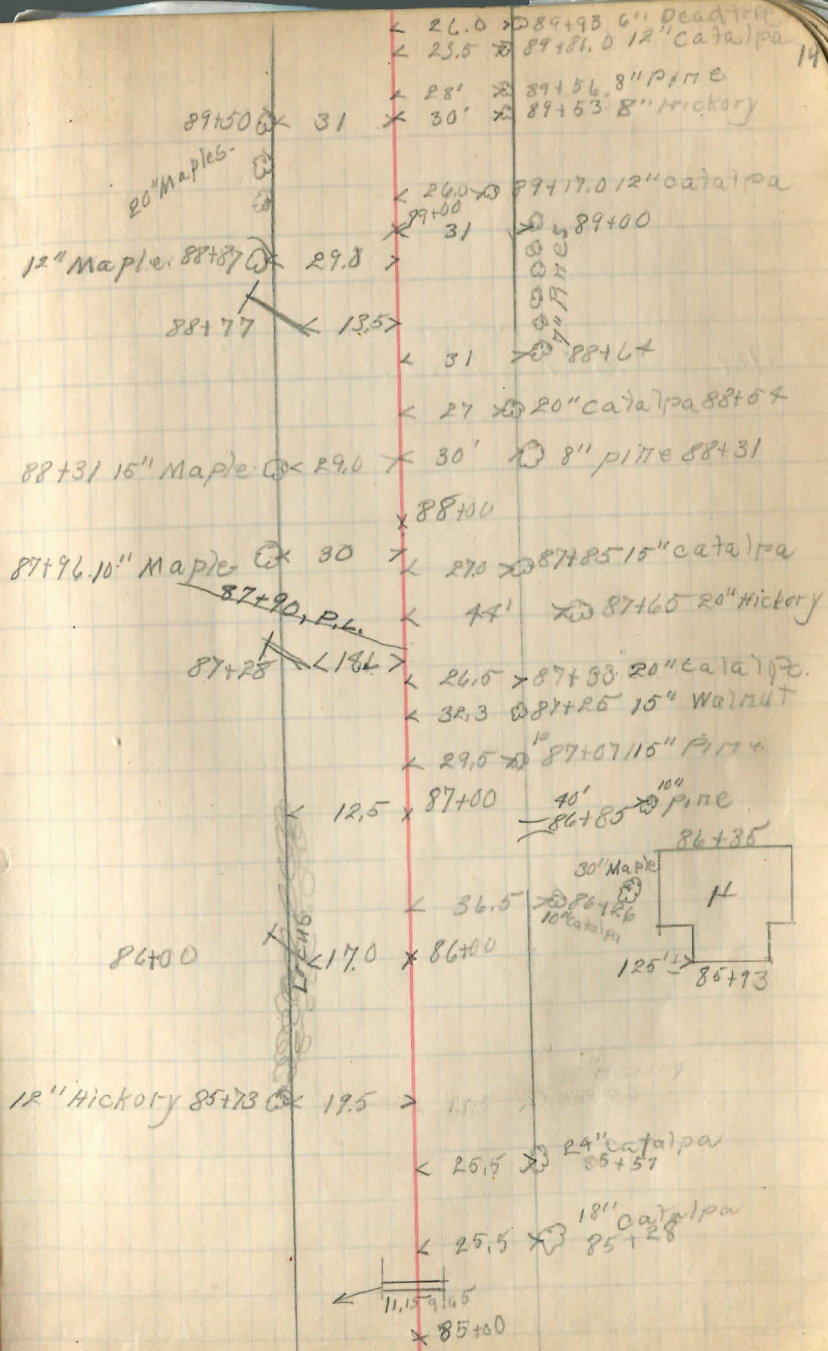
X 63+00



80+00 A = 21° 53' Left Curve Notes 15 pages over



85+23.5 2 1/2 x 2 1/2 Stone Box fair  
 Extend inlet and with } Concrete, Slab, Top  
 " " outlet " " } Type



26.0 x 89+93 6" Dead tree  
 25.5 x 89+81.0 12" Catalpa  
 28' x 89+56.8" pine  
 30' x 89+53.8" Hickory

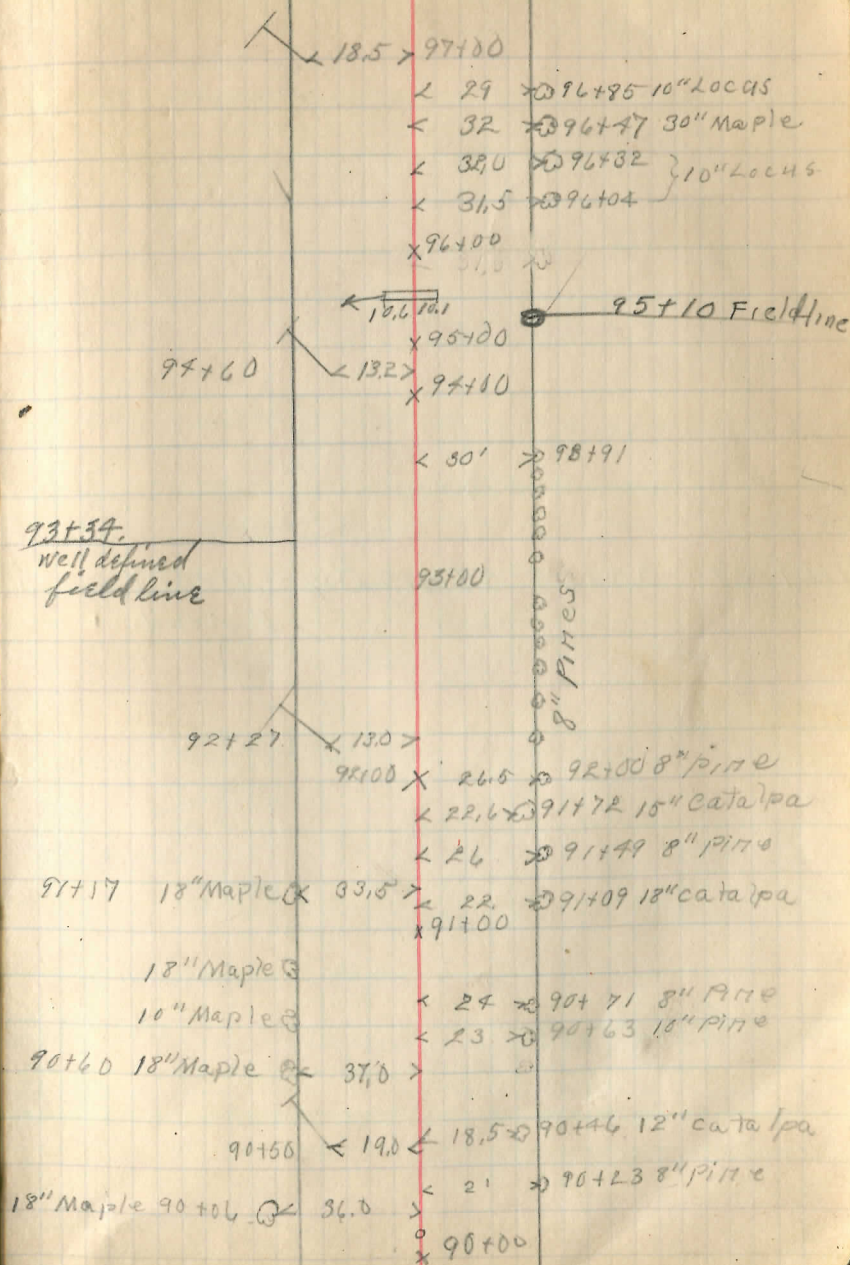
89+50 x 31 x 30' x 89+53.8" Hickory  
 20" Maple  
 12" Maple 88+87 x 29.8  
 88+77 x 13.5  
 88+31 15" Maple x 29.0 x 30' x 8" pine 88+31  
 88+10  
 87+96.10" Maple x 30' x 27.0 x 87+85.15" catalpa  
 87+90, P.L.  
 87+28 x 19.7  
 26.5 x 87+93 20" catalpa  
 32.3 x 87+25 15" Walnut  
 29.5 x 87+07 11" Pine  
 12.5 x 87+00  
 40' pine  
 86+85  
 86+35  
 30' Maple  
 86+00  
 10" Catalpa  
 17.0 x 86+00  
 125' x 85+93  
 12" Hickory 85+73 x 19.5  
 26.5 x 85+57 24" catalpa  
 25.5 x 85+28 18" catalpa  
 11.5 x 1.65  
 x 85+00

95+18.9

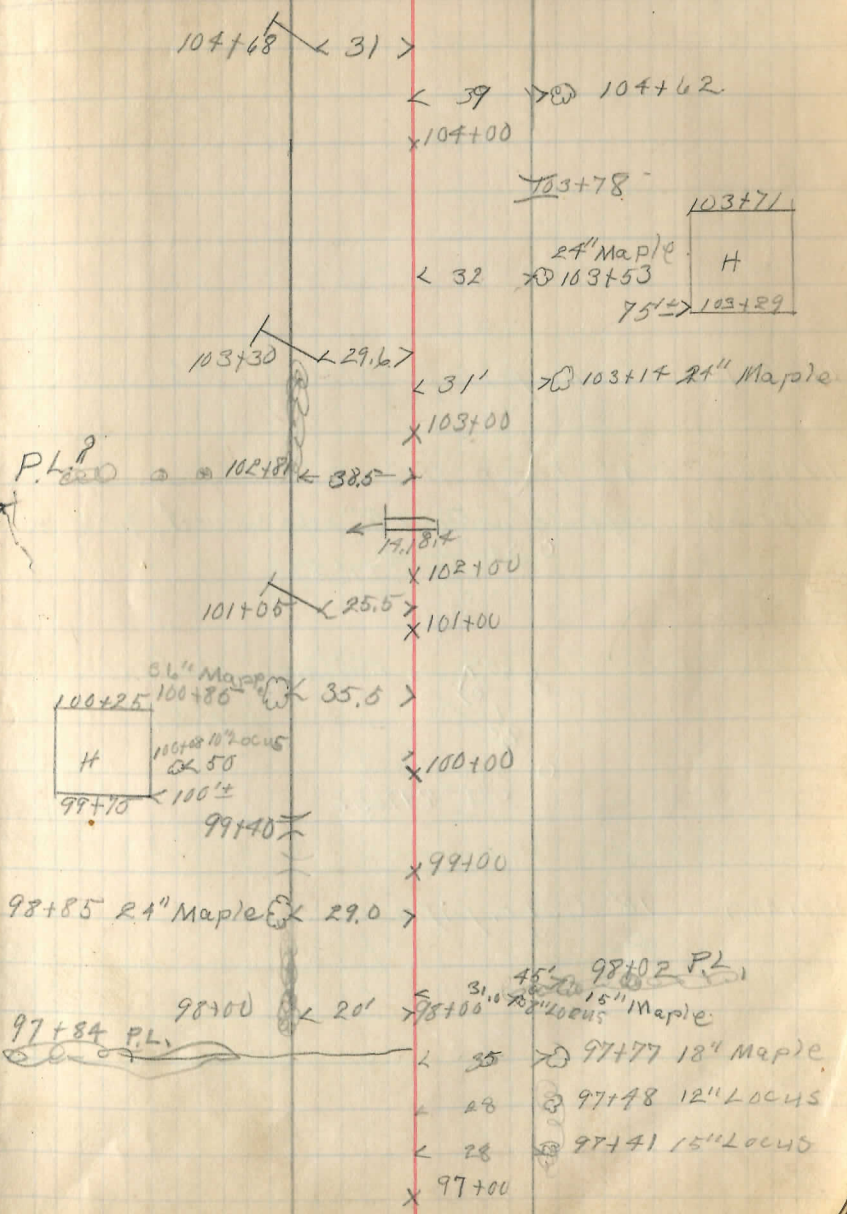
2'8" x 1'6" } good, extend.  
~~2.5 x 1~~ Stone Box Culvert

90+08.1

$\Delta = 20^{\circ} 58'$  R Curve Notes 14 pages over.

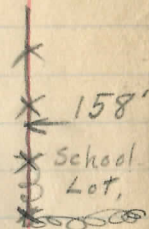


102+20.9 3.5x1.5 stone Box Culvert, Good.  
Extend.





20'± X 16"± stone box, Dilapidated  
 Requires 4' X 3' Culvert,



118+52.9 ~~2.5 X 2.5~~ stone box culvert, Fair.  
 2'8" X 2'± Part of slab has been  
 replaced with concrete. Extend

County line

123+96 8" Maple  $\times$  23 >  
 123+50 8" Maple  $\times$  23 < 29.5  $\times$  123+38 10" Maple  
 123+23 8" Maple  $\times$  23 >  
 $\times$  123+00

122+95 12" Catalpa  $\times$  22 >  
~~6 2~~ < 20 > 122+92 122+84  
S  
50.5, 122+58

122+54 18" Maple  $\times$  22.2 >

122+45 P.L. ~~25.0~~ >

$\times$  122+00

121+00

< 18.0 > 120+50

$\times$  120+00

$\times$  119+00

118+82 30" Elm  $\times$  25.5 < 26.0  $\times$  118+86 15" Maple

12.15 11.75  
 $\times$  118+00

$\times$  117+00

116+30 < 10' >

$\times$  116+00

115+38  
 Field Line

< 17.5 > 115+71

$\times$  115+00

125+12.65

End of Project notes 11 pages over  
pg 30

End of Project 125+12.65

X125+00

124+68 18" Maple  
X 46.5 >

124+85 24" Apple X 25.5 >

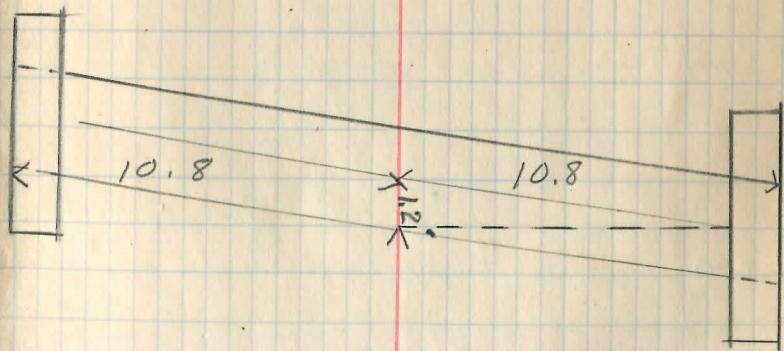
124+16 10" Maple X 23.2 >

124+06 20" Maple X 38.5 >  
X124

X124+60 18" Maple

< 31

68+30.



# MONUMENTS

43+00

32+00

24+00

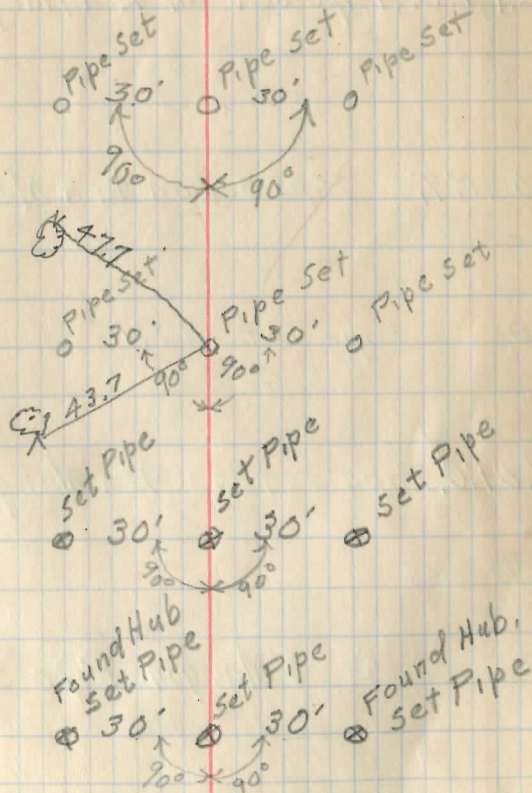
15+00

0+00

Found  $\frac{1}{2}$  Spike, replaced it with Iron

Feb. 3, 1931, P.M., Fair, 35°  
 Marks, Parks, Snyder, Merritt

21



Pipe

⊗

Feb. 4, 1931, Fair, 30° N.W. Wind,  
Marks, Parks, Snyder, Merritt.

90+08.1 Pipe Set at P.I.

89+02.1, P.C., Pipe set on  $\pm$  + Margins

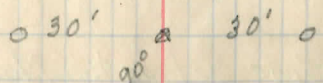
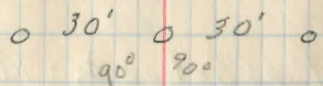
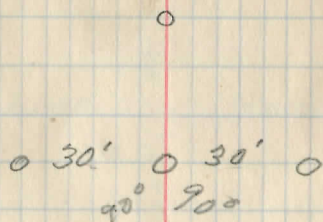
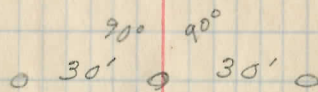
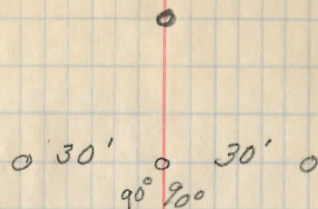
81+06.5, P.T., Pipe set on  $\pm$  + Margins

80+00 Pipe Set at P.I.

78+91.0 P.C. Pipe set on  $\pm$  + Margins

73+00  $\pm$  + Margin Pipe Set,

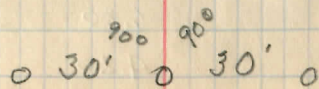
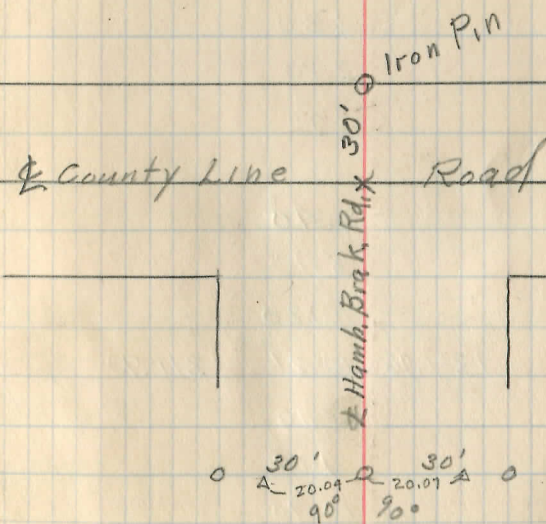
49+50  $\pm$  + Side Line Pipes Set.



125+42.65

125+12.65

110+00

Pipe Set on  $\star$  + Margins.91+118, P.T., Pipe Set on  $\star$  + Margins

22 July 55 C.M. 22

24

	+	HI	-	Elev
B.M.	11.00	1305.45		1294.45
T.P.	11.45	1316.36	0.54	1304.91
T.P.	7.47	1321.91	1.92	1314.44
B.M.			2.20	1319.71
Int. of 40 of 166 & Brakeman Rd.			4.20	17.7
Int + 100' W			3.40	
" + 200' W			2.60	
" + 300' W			1.60	
" + 400' W			1.50	
" + 500' W			2.70	
" + 600' W			3.90	
" + 100' E			6.40	
" + 200' E			8.10	
" + 300' E			10.20	11.7
T.P.	0.06	1311.76	10.21	1311.70
Int + 400' E			3.10	08.66
" + 500' E			7.10	
" + 600' E			10.70	
B.M.	1.90	1321.61		1319.71
1700			6.80	1314.81
begin pvc.			4.20	

W root 15" Maple 25' Rt of Sta 11+02  
Brakeman Rd.

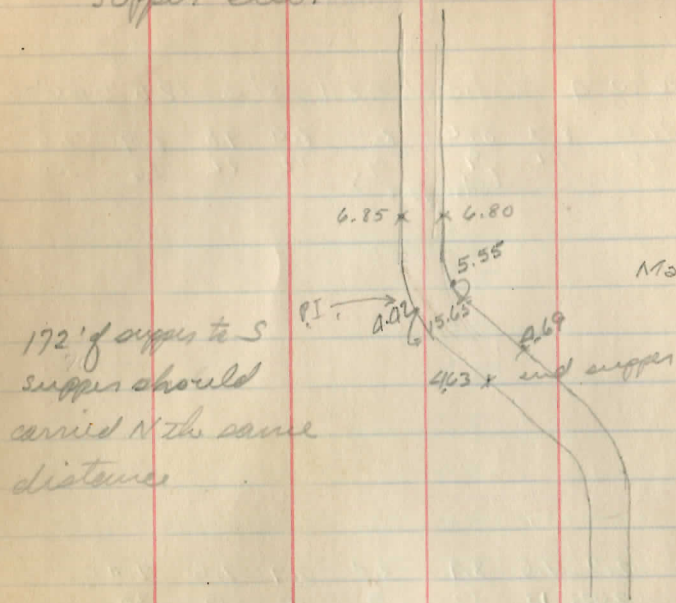
State highway monument ± 60' W of  
SR 166 & Brakeman Rd. (N side SR 166)

N					SR 166	S				
1.7	2.1	4.0	3.6	3.15	3.1	3.6	100' W of			
30	25	21	20	10.8	9.3	30	Brakeman			
5.5	6.2	7.0	6.4	6.2	6.2	6.5	100' E			
30	21.5	15	12	9.5	9.0	10.5	20 & 30 of			



W  
supper elev.

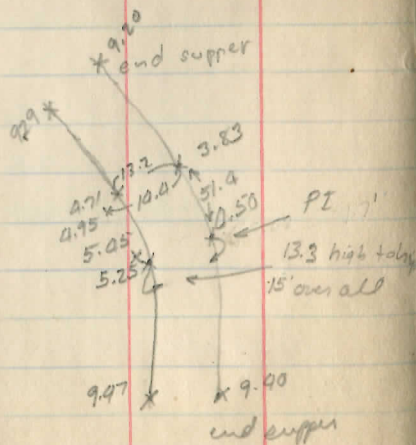
E



172' of supper to S  
supper should  
be carried N the same  
distance

Max 1.13''

207' of supper to N



.88 max

0.75

.07

124' of supper to S.



P.T, 81+06.5 10°46 1/2'

81+00 10°27'

80+50 7°57'

P.I, 80+00

A = 21°33' Left.

D = 10°00'

80+00 5°27'

T = 109.0'

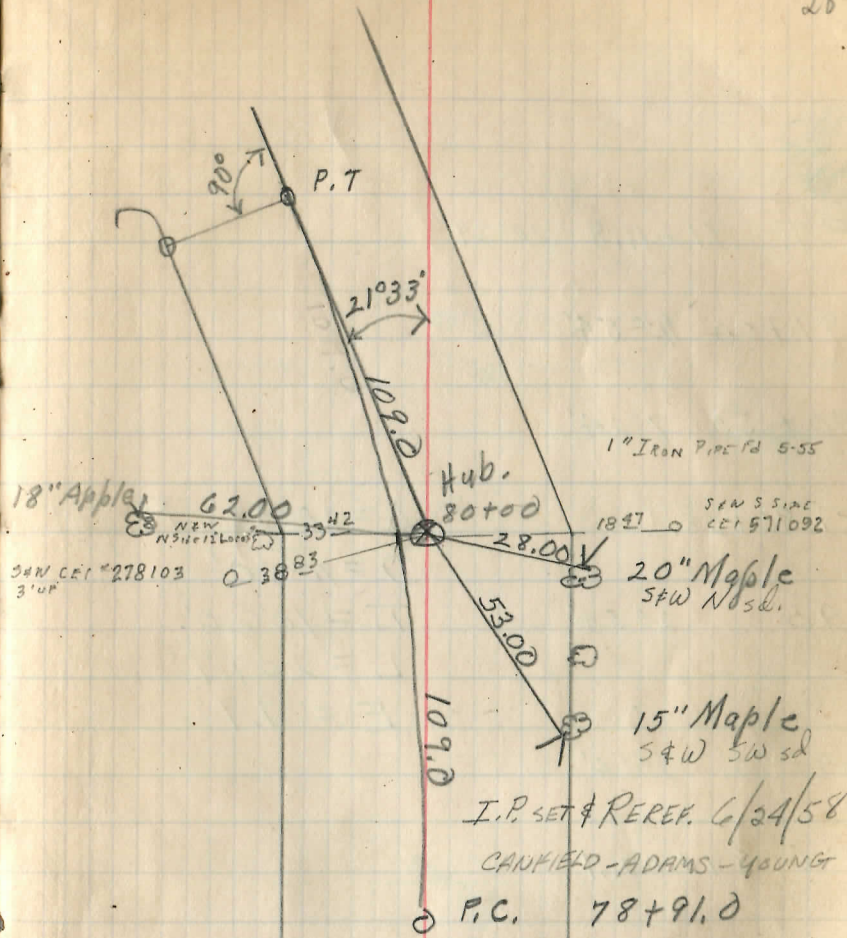
79+50 2°57'

L = 215.5'

E = 10.3'

79+00 0°27'

P.C. 78+91.0 0°27'



92+00

88.2

P.T. 91+11.8 10°29'

91+00 9°54'

90+50 7°24'

P.I. 90+08.1

90 2°54'

89+50 2°24'

P.C. 89+02.1

$\Delta = 20^{\circ}58'$  Right

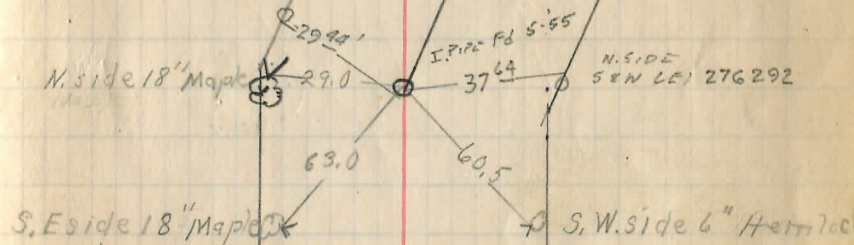
$D = 10^{\circ}00'$

$T_1 = 106.0'$

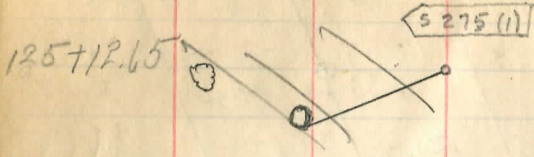
$L = 209.7'$

$E = 9.7'$

S. S. of  
S4 W 1/4 Sec 27 T27 R34

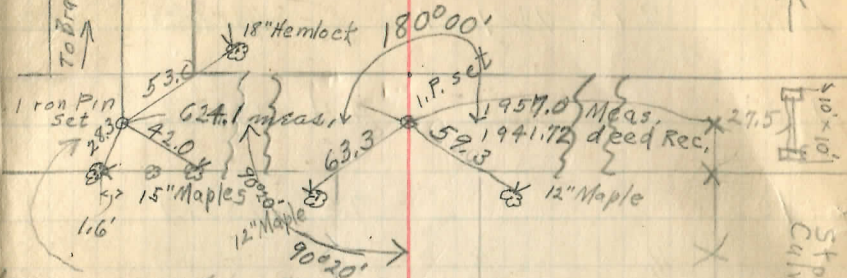


No FIND  
6/29/58



116 + 00

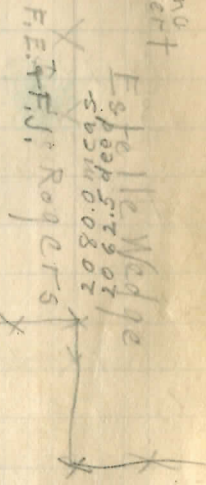
To Drakemoor Church



89 + 15.5 (pland)

No FIND  
4/24/58

D. CANFIELD  
T. ADAMS  
P. YOUNG



Hand 30' 30' 11/12

SPK. S.E. 5.30  
C.E.I. 860019

SPK. W. Side  
Gate Post

SPK. E. Side 21"  
Maple

180° R.R. SPK  
Set St. 52+32.22

Sign Post  
180°  
0.00

SPK. Crooked  
10" Fir  
1. P.W. fd. + used  
St. 28+66.03

SPK. C.E.I.  
267951

Callow Rd.

Radcliffe Rd

Lake Co.

Geauga Co.



S.R. 608

1. P. fd. St. 0+00  
+ used.

St. 95+58.79

Mod. box  
+ 112.10 fd. + used

Brakeman Rd  
Geauga Co

S.R. 86

1. P. fd. + used

Brakeman Rd  
Lake Co

90° 08' 00" Rec.

90° 13' 05" Obs.

629.12' Rec.  
+ obs.

SPK. N.E. 18" MAP.

33.17

179° 48' 05" R.R. SPK, set

89+34.67

SPK. N.W.  
C.E.I. # 574914

SPK. S. side  
18" MAP

F. JANEK  
BSL-497

21.40

54.80

M.T. + L.A.  
Grantham  
79+330  
24" MAP.

PIR

29.05

33.35

SPK. S.W.  
24" MAP.

180°  
R.R. SPK  
Set

St. 74+00.36



Lake Co.

Geauga Co

180°

St. 52+32.22

Cross sections

Table 21  
E1

BM	2.18	1321.61	1319.43
0+00		4.4	1317.2
1+10		7.5	1314.1
2		8.9	1312.7
3	T.P. 2.14	1313.35	1310.91
		4.2	1309.2
4		7.0	1306.4
5		8.7	1304.7
6	T.P. 3.82	1306.86	1303.04
		3.4	1303.6
7		5.4	1301.5
8		6.9	1300.0
9		8.5	1298.4
10		11.9	1295.0
	T.P. 3.12	1297.01	1293.89
11		4.6	1292.4

Fair

D. Parks  
R. H. Goodrich  
R. Hassel

June 21, 1929 80°

B.M. 24" Maple, E. Root, 24" Maple, 60± W. of Sta. 0+00

200.0	150.0	100.0	50.0	200.0	150.0	100.0	50.0	200.0
5.2	5.7	7.0	8.6	8.1	7.5	7.1	5.7	5.7
30.0	25.0	11.0	8.0	6.5	4	14.0	20.0	30.0
8.0	8.2	9.0	10.5	9.7	8.9	9.4	10.0	8.7
30.0	14.5	10.5	8.5	8.0	4	8.5	10.5	15.0
1.7	2.5	5.7	4.4	4.2	4.7	5.6	3.6	1.6
30.0	15.5	9.0	7.0	4	9.0	10.5	10.0	30.0
6.5	6.3	7.3	7.9	7.0	7.9	7.4	6.0	
30.0	25.4	12.0	8.5	4	7.0	8.5	30.0	
8.0	9.1	8.9	9.0	8.7	9.3	10.2		
30.0	13.0	10.5	9.0	4	6.0	30.0		
29.7	12.9	10.4	8.9	0.1	6.1	30.1		
1.9	2.0	4.0	7.9	9.0	3.5	4.2	3.5	
30.0	25.3	13.0	11.0	8.5	4	6.5	30.0	
29.7	24.9	12.9	10.9	8.4	0.1	6.6	30.1	
2.6	3.2	5.1	6.6	0.4	5.4	5.8	5.0	4.7
30.0	21.0	15.0	11.0	8.0	4	5.0	7.5	30.0
29.8	20.9	12.9	10.9	7.9	0.1	5.6	7.6	30.1
1.7	5.0	6.7	8.8	7.2	6.9	6.7	7.7	5.3
30.0	25.6	14.0	13.5	10.0	4	6.5	8.5	30.0
28.8	24.8	16.8	13.3	9.8	0.2	4.7	6.2	8.7
2.6	7.8	10.4	9.0		8.5	8.7	9.7	7.3
30.0	10.5	14.5	13.0		4	3.5	4.5	9.0
29.8	12.3	17.3	12.8		0.2	3.7	4.7	9.2
	9.5	14.0	12.2	11.9	12.0	13.4	9.6	8.2
30.0	25.0	12.0	13.0	4	2.5	3.5	12.0	15.0
29.8	22.8	14.8	12.8	0.2	2.7	3.7	10.2	15.2
5.6	4.7	5.0	4.1	4.6	4.9	2.5		
30.0	11.5	10.5	7.8	4	10.0	30.0		
29.8	11.3	10.3	9.3	0.2	10.2	30.2		



21		1304.79	6.7	1298.1
T.P.	7.72	1306.65	5.56	1299.23
22		(1308.34)	6.3	1300.4
B.M.	4.65	1308.34	2.96	1303.69
23			5.8	1302.5 <del>1300.9</del>
24			4.4	1308.9 <del>1302.4</del>
25		1303.63V	6.8	1301.5 <del>1300.0</del>
	4.23	1301.94	8.94	1299.40V <del>1297.71</del>
26			4.0	1299.6 <del>1297.7</del>
27			4.8	1298.8 <del>1297.1</del>
27+06			4.8	1298.8 <del>1297.1</del>
28			4.4	1299.2 <del>1297.5</del>
28+70			2.0	1301.6 <del>1297.9</del>
T.P.	4.55	1305.0W 1303.32	3.17	1300.4V <del>1298.77</del>
29			3.9	1301.1 <del>1299.4</del>
30			5.5	1299.5 <del>1297.8</del>
30+36.4	8" corr iron pipe		5.2	1299.8 <del>1295.1</del>

x	x	x	x	-	-	-	-	-	-	x	x
36	3.6	7.4	6.4	8.0	6.9	6.7	7.0	7.4	7.3	7.2	
<del>26.6</del>	<del>19.6</del>	<del>7.6</del>	<del>5.6</del>	<del>3.6</del>	<del>1.1</del>	<del>0.4</del>	<del>11.4</del>	<del>12.9</del>	<del>17.9</del>	<del>30.4</del>	
4.3	4.3	5.7	7.7	6.3	6.3	6.7	6.5	5.7	5.3		
<del>30.0</del>	<del>22.1</del>	<del>5.6</del>	<del>1.6</del>	<del>0.5</del>	<del>0.4</del>	<del>13.4</del>	<del>14.4</del>	<del>15.9</del>	<del>30.4</del>		
Bent Spike E. Foot 12" Maple 25" Lt Sta. 22+70											
4.8	5.7	6.0	6.9	6.3	5.8	6.2	6.7	6.9	6.4		
<del>29.5</del>	<del>14.5</del>	<del>6.5</del>	<del>5.0</del>	<del>2.5</del>	<del>0.5</del>	<del>12.5</del>	<del>13.5</del>	<del>14.0</del>	<del>15.0</del>	<del>30.5</del>	
3.3	2.7	4.0	3.3	4.4	4.2	4.8	5.1	4.2	3.3		
<del>29.5</del>	<del>24.5</del>	<del>8.5</del>	<del>6.5</del>	<del>0.5</del>	<del>2.5</del>	<del>12.5</del>	<del>14.0</del>	<del>15.0</del>	<del>30.5</del>		
5.8	5.2	5.2	7.9	7.3	6.8	7.3	7.7	4.9	3.8		
<del>29.5</del>	<del>24.5</del>	<del>10.5</del>	<del>4.5</del>	<del>5.0</del>	<del>0.5</del>	<del>10.5</del>	<del>12.0</del>	<del>18.5</del>	<del>30.5</del>		
4.5	4.4	4.2	4.8	4.0	4.3	4.6	4.0	3.7	4.4	1.6	
<del>29.5</del>	<del>24.5</del>	<del>9.5</del>	<del>7.5</del>	<del>0.5</del>	<del>8.0</del>	<del>10.5</del>	<del>12.5</del>	<del>10.0</del>	<del>19.5</del>	<del>30.5</del>	
4.5	5.6	5.9	5.3	4.8		5.1	6.1	5.0	5.6		
<del>29.5</del>	<del>10.5</del>	<del>9.5</del>	<del>7.5</del>	<del>0.5</del>	<del>5.0</del>	<del>9.0</del>	<del>14.5</del>	<del>14.5</del>	<del>30.5</del>		
12.981	12.970	14.61	14.67	14.91	12.92	5.5	12.55	14.45	12.991	12.92	30.5
3.8	4.9	6.2	5.2	4.8	5.7	6.4	7.4	7.8	9.7	10.1	
<del>10.0</del>	<del>30.0</del>	<del>8.0</del>	<del>8.0</del>	<del>0.5</del>	<del>8.0</del>	<del>50.0</del>	<del>100.0</del>	<del>200.0</del>	<del>260.0</del>		
99.5	49.5		8.0		0.5	8.0	50.0	100.0	200.0	260.0	
1.3	2.4	5.4	7.8		4.4	5.1	2.4	2.1			
<del>30.0</del>	<del>7.0</del>	<del>9.5</del>	<del>6.5</del>		<del>10.5</del>	<del>18.0</del>	<del>30.0</del>				
29.4	16.4	8.9	5.9		0.6	11.1	18.6	30.6			
1.1	1.5	3.5	4.9	4.2	3.9	4.2	3.2	2.6			
<del>30.0</del>	<del>20.0</del>	<del>10.0</del>	<del>5.0</del>	<del>5.0</del>	<del>0.5</del>	<del>13.0</del>	<del>21.0</del>	<del>30.0</del>			
29.4	21.4	9.4	7.9	4.9	0.6	13.1	21.4	30.6			
4.2	5.0	5.6	5.5		5.7	5.8	5.1	5.5			
<del>30.0</del>	<del>14.0</del>	<del>8.0</del>	<del>4.0</del>		<del>10.0</del>	<del>12.0</del>	<del>15.0</del>	<del>30.0</del>			
29.4	9.9	7.4	0.6		10.6	13.1	15.6	30.6			
4.2	4.2	5.2			5.8	6.6	7.2	5.6	11.0		
<del>30.0</del>	<del>10.0</del>	<del>5.0</del>			<del>13.0</del>	<del>50.0</del>	<del>100.0</del>	<del>200.0</del>			
49.6			0.6		13.6	50.6	100.6	200.6			

1305.01  
1303.82

31 B.M. 5.85 1306.11 ✓ 5.2 1298.1  
1304.42 4.75 1300.26 ✓ 1299.57

32 5.7 1300.4  
1298.7

33 6.0 1301.1  
1299.4

34 7.6 1298.5  
1296.8

T.P. 4.7+ 1302.97 ✓ 7.88 1298.23 ✓  
1301.28 4.7 1296.57  
1298.3  
1296.6

35 4.7 1296.6

35+07 4.8 1298.2  
1296.5

6.65 1304.82 ✓ 4.80 1298.17 ✓  
1303.13 6.7 1296.78  
1298.1  
1296.4

36 6.7 1296.4

37 8.8 1296.0  
1294.3

J 8.5 1296.3  
1294.6

37+89

38 8.7 1296.1  
1294.4

6.68 1304.72 ✓ 4.78 1298.04 ✓  
1303.03 1296.35  
1298.1

39 6.6 1296.4  
1301.06 ✓

8.37 1309.43 ✓ 3.66 1299.37  
1301.16

40 7.8 1294.7

3.0 4.8 5.2 5.0 5.6 5.2 5.1  
30.0 17.0 2 7.5 16.5 19.0 24.0  
29.4 13.4 0.6 8.1 17.1 19.6 27.6

North West Root 18 Maple 27 Pt. Sta. 31+98  
30+98

17 25 4.3 4.7 5.7 7.8 7.7 5.1 5.5 7.0 3.8 3.7  
30.0 15.0 7.5 8.0 2 2.8 7.5 17.0 18.0 20.0 25.0 30.0  
29.4 17.4 8.9 2.4 0.6 2.6 10.4 17.6 18.6 20.6 25.6 30.6

3.2 4.5 5.1 5.0 4.6 5.3 5.6 5.3 6.1  
30.0 1.0 3.0 2 10.5 17.5 19.0 21.0 30.0  
29.3 5.3 2.3 0.7 11.2 18.2 19.7 21.7 30.7

1.3 2.0 6.0 5.7 7.6 6.6 6.2 6.7 7.2 5.5 7.9 7.4  
30.0 15.0 8.0 3.5 2 2.0 10.0 17.0 17.0 21.0 26.0 30.0  
29.3 17.3 7.3 2.8 0.7 2.7 10.7 17.7 19.7 22.2 25.7 30.7

4.4 5.0 5.5 6.6 5.1 4.7 5.2 7.2  
30.0 20.0 17.0 8 7.0 30.0  
29.3 24.3 10.3 7.3 4.8 0.7 19.7 30.

28.4 1298.4 1298.2 1298.6 1298.6 1298.6 1298.6 1298.6 1298.6 1298.6 1298.6 1298.6  
30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0 30.0  
49.3 29.3 2.3 1.3 0.7 16.7 18.2 50.7 100.7 150.7

0.8 1.7 4.3 6.7 6.7 6.9 7.8 6.8 4.2 4.1  
30.0 18.5 5.5 2 11.0 17.0 20.0 20.5 25.0 30.0  
29.3 17.8 4.8 0.7 10.7 18.7 20.7 23.2 25.7 30.7

7.1 5.1 8.8 7.9 9.3 8.8 9.2 10.3 11.3  
30.0 20.0 17.0 8 7.0 30.0  
34.3 24.3 11.3 7.8 2.8 0.7 15.2 19.2 30.7

1096.9 1094.6 1091.7 1091.3 1091.6 1091.0 1091.3 1091.3  
7.2 5.6 11.4 10.4 8.8 8.5 9.1 10.7 11.8 12.6 14.3

100.0 57.0 11.0 10.5 50.0 100.0 150.0  
99.3 44.3 10.3 0.7 11.2 50.7 100.7

8.2 9.3 9.3 10.4 9.1 8.7 9.0 9.7 9.8 11.1  
30.0 25.0 15.0 10.5 7.5 2 14.0 14.5 16.0 30.0  
29.2 24.2 12.2 9.7 6.7 0.8 10.8 13.3 16.8 30.8

3.2 3.1 8.1 6.9 6.6 7.1 7.9 3.1 2.8  
30.0 25.0 17.0 9.0 2 6.0 8.0 17.5 30.0  
29.2 24.2 10.2 8.2 0.8 6.8 8.8 13.3 30.8

6.8 7.8 9.4 8.4 7.8 8.4 7.7 7.9  
30.0 16.0 7.0 17.0 4 9.5 16.0 30.0  
29.2 19.2 8.2 6.7 0.8 7.4 11.8 30.8

	1309.43 ✓ <del>1367.74</del>		1302.7
411		6.7	<del>1301.0</del>
			1304.5
42	1309.27 ✓	4.9	<del>1302.8</del> ✓
	4.84	5.00	<del>1304.43</del> ✓
			<del>1302.74</del>
43		4.2	<del>1305.1</del>
			<del>1303.4</del>
			1305.41 ✓
B. M.		3.86	<del>1303.72</del>

+	+	+	-	-	-	-	+	+
7.1	7.5	6.7	7.8	7.3	6.7	7.2	6.5	5.5
<del>50.0</del>	<del>24.0</del>	<del>11.5</del>	<del>8.5</del>	<del>7.0</del>	<del>2</del>	<del>7.0</del>	<del>11.0</del>	<del>36.0</del>
29.2	29.2	10.7	7.7	6.2		0.5	9.8	11.8
								30.8
+	+	+	-	-	-	-	+	+
3.5	3.9	5.3	6.1	5.8	4.9	5.6	5.1	5.0
<del>50.0</del>	<del>22.0</del>	<del>7.5</del>	<del>9.5</del>	<del>7.5</del>	<del>X</del>	<del>7.5</del>	<del>11.0</del>	<del>25.0</del>
29.2	21.2	9.7	8.7	6.7		0.8	10.3	11.8
								25.8
								30.8
+	+	+	-	-	-	-	+	+
3.4	4.6	5.1	4.2	4.2	4.2	4.8	5.3	
<del>34.0</del>	<del>17.0</del>	<del>9.5</del>	<del>2.0</del>	<del>2.0</del>	<del>2.0</del>	<del>9.5</del>	<del>30.0</del>	
29.1	11.1	8.6				10.4	30.9	

R.P. Spike North West side trunk 10" Maple 28' Rt.  
Sta. 73+20

Stopped June 21, 1929

B.M.	3.82	1309.23 ✓ 1307.54	1305.41 ✓ 1303.72
44			1304.3 <del>1307.6</del>
45		1303.87 ✓ <del>1302.18</del>	1302.6 1300.9 1399.53 ✓ 1297.54
T.P.	4.34		1299.0 <del>1297.3</del>
46			4.9
47			1294.3 <del>1292.6</del>
T.P.	4.06	1296.92 ✓ 1295.23	1292.86 ✓ 1291.17 1292.15
48			1290.7 <del>1290.5</del>
48.08 ✓			1292.2 1290.5
49			1292.0 <del>1290.3</del>
49+45			1292.9 <del>1291.2</del>
T.P.	2.91	1295.44 ✓ 1293.75	1292.53 ✓ 1290.84 1289.9 <del>1288.0</del>
50			5.5
51			9.7 1285.7 1284.1
52			1281.8 <del>1280.2</del>
T.P.	0.05	1283.57 ✓ 1281.88	1283.52 ✓ 1281.83 1274.0 1274.3 1271.02 <del>1269.33</del>
53			7.6
T.P.	3.25	1274.27 ✓ 1272.58	1271.02 <del>1269.33</del>

June 23 1929. Cloudy 70°  
D. Parks 36  
R. H. Goodrich  
R. Hassel

R. P. spike North West Trunk 10" Maple 28'

Rt. Sta. 43+20

+	+	+	-	-	-	-	-	-	-
4.0	4.4	4.7	6.2	5.2	4.9	5.2	6.3		
30.0	25.0	12.5	9.0	7.0	4	8.0	30.0		
+	+	-	-	-	-	-	-	+	+
3.9	4.6	8.5	7.3	6.6	7.0	7.8	4.9	4.5	
30.0	18.0	9.0	7.0	4	6.5	8.0	12.0	30.0	
+	+	-	-	-	-	-	+	+	+
2.3	3.4	5.2	4.9	5.3	6.1	2.3	1.6	1.9	
30.0	16.0	7.0	4	6.0	8.0	15.0	25.0	30.0	
+	-	-	-	-	-	+	+	+	+
7.1	7.8	10.8	10.3	9.6	10.1	9.7	9.1	7.8	7.9
30.0	16.5	12.0	9.5	4	8.0	11.0	15.0	25.0	30.0
-	-	-	-	-	-	-	-	-	-
5.1	4.8	5.5	4.5	4.4	4.5	5.1	7.0		
27.0	17.0	16.5	12.0	4	6.0	7.0	30.0		
1290.7	1290.5	1290.0	1289.9	1289.2	1288.5	1287.8	1287.2	1286.5	1285.8
4.5	6.5	7.7	4.2	4.7	5.1	5.2	6.5	7.0	8.0
30.0	15.0	13.5	4	4.5	5.0	5.0	50.0	100.0	
+	+	+	-	-	-	+	+	+	+
1.9	2.8	4.5	5.6	5.1	4.9	5.0	4.7		
30.0	25.0	18.0	16.0	10.5	4	8.5	30.0		
+	+	+	-	-	-	+	+	+	+
2.0	3.1	4.7	6.2	5.6	5.5	5.4	4.7	3.7	
30.0	25.0	18.5	16.5	14.0	4	14.0	16.0	30.0	
+	+	-	-	+	-	+	+	+	+
4.6	9.2	10.5	9.7	9.3	9.7	10.4	9.2	8.0	
30.0	18.5	17.5	13.5	6.0	4	2.5	3.5	30.0	
+	+	-	-	-	-	+	+	+	+
11.8	12.2	14.8	13.7		13.6	15.0	12.5	11.9	
30.0	24.0	17.0	14.0		4	2.0	3.6	30.0	
+	+	+	-	+	-	+	+	+	+
3.6	5.8	5.9	8.7	7.4	7.6	8.1	4.6	2.9	
30.0	25.0	22.0	19.5	16.0	4	1.5	7.5	30.0	

54		1274.27V 1272.58	4.1	1270.2 <del>1268.5</del>
55			8.8	1265.5 1263.8
56	2.40	1265.37V 1263.68	11.30	1262.97V 1261.28
B.M			3.5	1261.88
57			3.49	1260.19
			5.9	1259.5
58			8.6	1256.8 1250.1
59			10.4	1255.0 1253.3
60	2.16	1254.30V 1254.61	11.23	1254.14V 1252.45
61			4.1	1252.2 1250.5
62			8.2	1248.1 1246.4
63			10.7	1245.9 1243.9
64	3.17	1246.37V 1244.68	13.10	1243.20V 1241.51
B.M.			2.6	1243.8 1242.1
65			5.0	1241.4 1239.7
			3.25	1243.12V 1241.43
			8.6	1237.8 1236.1

1.2	2.8	7.8	3.7	4.1	4.5	1.8	0.3
30.0	25.0	19.0	16.0	2	1.0	6.0	30.0
7.1	7.0	7.4	9.8	8.8	8.8	10.0	7.3
30.0	25.0	20.0	17.5	15.5	2	2.0	2.5
0.1	1.7	4.8	3.7	3.5	4.2	2.5	1.9
30.0	21.5	12.0	15.0	2	2.0	5.0	29.0
Spike S.W. side 12" W. Chem 30' Pt Sta. 56+70							
6.1	6.1	5.7	7.0	6.4	5.9	7.2	5.4
30.0	26.0	18.0	15.0	13.5	2	3.0	6.5
8.7	8.4	10.0	8.7	8.6	9.0	10.2	7.3
30.0	17.0	15.0	12.0	2	1.0	2.5	8.0
10.8	10.4	12.3	10.9	10.4	10.8	12.8	10.4
30.0	17.0	15.5	13.0	2	1.0	2.5	7.0
3.4	3.5	6.2	4.6	4.1	4.3	6.3	2.3
30.0	19.1	16.0	13.5	2	1.5	3.0	11.0
5.9	6.3	9.6	8.6	8.2	7.7	8.8	5.8
30.0	15.0	16.5	14.5	2	3.0	7.0	12.0
9.7	11.6	12.0	10.9	10.7	11.2	12.0	9.2
30.0	19.0	15.5	12.0	2	1.5	3.0	9.0
2.2	2.2	4.3	3.1	2.6	2.8	4.1	2.4
30.0	12.0	15.0	13.0	2	1.5	2.5	5.5
2.4	5.1	4.4	5.1	5.0	5.3	6.7	5.3
30.0	16.5	14.5	10.5	2	2.0	4.5	8.0
S.W. side trunk 24" pine 22' Pt. Sta. 64+13							
5.9	7.3	8.6	8.0	7.3	8.1	6.6	7.0
30.0	15.0	2	5.0	8.0	10.0	13.0	25.0

		1246.37 ✓		1237.01 ✓
		<del>1244.68</del>		<del>1232.32</del>
TP	6.08	1240.89 ✓	12.84	1231.7
66.		<del>1238.46</del>		1230.0 ✓
			8.4	1227.14 ✓
TP	8.35	1235.51 ✓	12.93	<del>1225.47</del>
66+88		<del>1233.82</del>		1224.3
			11.2	<del>1222.6</del>
67				1223.6
			11.9	1221.9
T.P.	2.31	1225.65 ✓	12.17	1223.34 ✓
T.P.		<del>1223.96</del>		<del>1221.65</del>
			3.45	1222.20 ✓
				<del>1220.51</del>

11.5	3.0	10.3	7.7	9.7	8.6	10.9	4.8	6.0	6.5
<u>35.0</u>	<u>18.5</u>	<u>8.5</u>	<u>5.5</u>	<u>2</u>	<u>8.5</u>	<u>11.5</u>	<u>15.0</u>	<u>23.0</u>	<u>30.0</u>
+	+	-	-	-	-	+	+	+	+
16.9	2.4	12.6	11.7	11.2	11.7	12.5	10.9	8.3	8.4
<u>30.0</u>	<u>25.0</u>	<u>9.5</u>	<u>7.0</u>	<u>2</u>	<u>6.5</u>	<u>13.0</u>	<u>17.0</u>	<u>25.5</u>	<u>30.0</u>
+	+	+	-	-	-	+	+	+	+
8.5	8.5	9.6	12.8	12.3	11.2	12.7	11.7	9.4	10.2
<u>30.0</u>	<u>25.0</u>	<u>16.0</u>	<u>8.0</u>	<u>6.0</u>	<u>2</u>	<u>15.0</u>	<u>17.0</u>	<u>27.0</u>	<u>30.0</u>

N.E. Cor, North Headwall)

July 5, 1929 In afternoon F. Braun

T.P.	3.56	1225.76 <del>1224.07</del> 3.4 4.4	1222.20 <del>1225.57</del>
68		4.3	1221.5 <del>1219.8</del>
68+30	Com, culvert	4.4	1221.4 <del>1219.7</del>
69		5.9	1219.9 <del>1218.2</del>
T.P.	10.13	1235.12 <del>1233.43</del>	1224.99 <del>1223.30</del>
70		12.0	1223.1 <del>1221.4</del>
T.P.	8.17	1242.09 <del>1240.40</del>	1233.92 <del>1232.23</del>
71		1.95	1231.6 <del>1229.7</del>
72		6.0	1234.1 <del>1231.9</del>
T.P.	9.69	1242.95 <del>1241.26</del>	1233.26 <del>1231.57</del>
B.M.		5.99	1234.76

1235.60

6.5	5.9	6.5	5.1	4.3	4.6	6.0	5.2	5.9	6.4
80.25	78.0	76.5	75.0	73.5	72.0	70.5	69.0	67.5	66.0
11.0	9.6	8.7	5.6	3.5	4.7	4.7	4.8	3.6	5.9
100.0	50.0	10.9	10.0	9.6	10.7	25.0	50.0		
7.9	7.7	6.3	4.3	5.9	5.9	6.3	5.7	6.0	6.7
30.0	25.0	11.0	5.5	5.6	6.5	12.0	16.5	18.0	30.0
10.8	9.1	10.1	11.2	13.2	12.2	12.0	11.9	12.6	9.8
10.8	24.5	11.0	12.0	9.0	6.5	6.8	8.0-10.0	14.0	22.0
9.9	9.9	11.2	10.8	10.5	10.2	11.5	9.5	8.1	4.7
30.0	9.5	10.0	5.0	8.0	10.0	11.0	12.5	17.0	26.0
6.0	6.0	5.8	6.7	6.0	6.2	7.0	5.9	4.6	4.6
30.0	25.0	11.0	6.5	9.0	12.0	13.5	26.0	30	

→ E. root 24" pine 16' Lt. sta. 73+10

Corrected Elevation:  
See Slope stake notes

Sun.  
Hot  
showers  
D. Parks  
P. Goodrich  
F. Gran.

July 6, 1929

		1241.59		1235.60
B.M	5.99	<del>1241.64</del> 1242.75		<del>1235.65</del> 1236.96
73			5.7	1235.9 <del>1237.3</del>
74			9.9	1231.7 <del>1233.1</del> 1228.53
T.P.	4.49	<del>1233.02</del> <del>1234.38</del>	13.06	1229.89
75			7.9	1225.7 <del>1221.1</del>
T.P.	6.20	<del>1226.25</del> <del>1227.61</del>	13.02	1220.00 <del>1221.36</del>
76			7.8	1218.5 <del>1219.8</del>
77			10.9	1215.4 <del>1216.7</del> 1213.92
T.P.	5.32	<del>1219.24</del> <del>1220.60</del>	12.33	<del>1215.28</del> 1215.6
78			7.8	<del>1212.8</del> 1214.2
78+72			5.0	1214.2 <del>1215.6</del> 1216.75
T.P.	10.01	<del>1226.76</del> <del>1228.12</del>	2.19	1218.11
79			12.2	1214.6 <del>1215.7</del>
79+80			9.5	1219.3 <del>1218.6</del>
80			6.0	1220.8 <del>1222.1</del>
80+50			5.1	1221.7 <del>1223.0</del>
81			6.5	1220.3 <del>1221.6</del>

6.1	5.7	6.1	5.8	5.7	5.9	5.5	3.6	2.21
30.0	12.0	9.0	7.0	4	3.5	9.0	17.5	30.0
7.7	9.1	10.5	10.0	9.9	10.2	10.9	9.2	8.0
30.0	14.5	15.0	11.0	9.0	5.5	7.0	7.5	30.0
3.7	4.8	5.7	8.9	7.6	7.3	7.4	8.4	5.8
30.0	18.0	13.8	9.0	7.5	4	4.0	9.0	10.5
9.0	4.7	6.3	7.0	8.9	8.3	7.8	8.2	9.1
22.5	12.5	13.7	10.0	8.5	4	4.5	9.0	4.1
4.2	12.0	11.4	11.8	11.3	10.7	10.9	11.1	11.5
50.0	17.0	13.0	10.0	8.0	3.0	4	3.0	4.6
8.1	7.8	9.3	7.4	5.3	7.8	5.1	5.8	8.1
30.0	22.0	19.0	7.0	3.0	4	3.5	6.0	17.0
14.2	11.5	10.5	7.5	5.3	5.3	5.0	5.4	5.6
50.0	30.0	30.0	7.1	9.6	4	6.5	8.1	12.0
9.1	9.7	12.7	11.9	12.2	12.7	9.2	7.5	7.0
30.0	24.0	16.0	8.0	4	3.0	8.1	25.0	30.0
6.4	7.4	9.1	10.1	9.6	9.5	9.6	10.1	8.7
30.0	19.0	13.0	14.0	10.0	4	20.0	9.5	13.0
5.6	5.1	4.6	6.9	6.5	4.0	6.7	6.4	5.3
30.0	21.0	18.0	7.5	5.5	4	6.5	9.5	12.0
5.9	5.3	5.1	5.6	5.1	4.7	5.0	5.3	4.8
30.0	15.0	4.5	3.0	4	5.5	12.0	14.0	7.0
5.4	5.7	7.0	6.5	6.1	6.5	5.6	5.3	
30.0	3.0	2.0	4	6.0	17.0	7.0	34.0	



		1210.95 <del>1212.81</del>		
91			5.1	1205.9 <del>1207.2</del> 1205.75
T.P.	3.09	1208.84 <del>1210.20</del>	5.20	<del>1207.11</del> 1205.0 <del>1206.4</del>
92			3.8	
93			6.1	1202.7 <del>1204.1</del>
94			8.7	1200.1 <del>1201.5</del>
95			9.0	1199.8 <del>1201.2</del>
95+P8.7			9.1	1199.7 <del>1201.1</del>
96			9.2	1199.6 <del>1201.0</del>
T.P.	8.96	1208.87 <del>1210.23</del>	8.93	1199.91 <del>1201.27</del> 1202.67 <del>1204.03</del>
B.M.			6.20	
97			7.4	1201.5 <del>1202.8</del>
98			6.3	1202.6 <del>1203.9</del>
99			8.9	1200.0 <del>1201.3</del>
100			10.2	1198.7 <del>1200.0</del>
T.P.	2.06	1198.50 <del>1199.86</del>	12.73	1198.44 <del>1199.80</del> 1195.5 <del>1196.9</del>
101			3.0	

4.6	5.1	5.3	5.7	5.3	5.1	5.5	6.2	5.0	3.9
30.0	25.0	11.0	12.0	9.0	4	6.5	8.5	11.0	30.0
9.7	4.0	4.6	4.3	3.8	4.3	5.7	3.7	2.7	2.5
30.0	11.0	9.0	6.0	4	7.0	9.0	12.0	26.0	30.0
5.1	5.3	7.3	6.5	6.1	6.6	8.0	7.5	5.5	3.1
31.5	10.0	6.5	7.0	4	7.5	10.0	11.0	13.5	30.0
9.0	8.7	9.2	8.7	8.8	9.6	8.6	6.7		
30.0	8.0	6.0	4	8.0	9.0	11.0	14.0	30.0	
11.3	10.7	9.7	11.2	9.7	9.0	9.3	10.8	9.4	9.7
30.0	18.0	13.0	11.5	8.5	6.5	4	11.0	13.0	16.0
13.9	11.6	10.5	8.3	9.2	9.1	9.0	7.9	10.3	12.1
30.0		10.8	9.0	4	7.5	10.1		50.0	100.0
9.2	9.6	10.1	9.8	9.7	10.1	9.5	7.6	7.1	
30.0	15.0	11.0	4	7.5	12.5	13.0	25.0	30.0	

W. root 30" Maple 30' RT sta 96+50

6.2	6.6	7.7	8.9	8.3	7.7	8.0	8.5	6.7	6.2	5.7	5.7
30.0	17.0	13.5	13.5	8.5	4	7.0	9.0	12.0	15.0	25.0	30.0
5.6	5.6	5.8	6.4	7.3	7.1	6.3	6.7	7.3	6.0	4.8	3.5
30.0	26.0	13.0	12.5	9.0	7.0	4	8.0	10.0	12.5	16.0	26.0
7.4	7.6	8.7	9.4	9.0	8.9	8.8	9.4	8.4	7.9		
30.0	25.0	11.5	8.0	5.0	4	9.0	12.0	14.5	30.0		
8.4	10.1	11.5	10.2	10.6	11.2	9.8	10.2				
30.0	10.0	8.0	4	8.0	11.0	14.0	30.0				
0.6	1.3	2.6	4.6	3.4	3.0	3.5	4.1	2.3	1.2		
30.0	25.0	15.0	12.0	9.0	4	6.0	8.0	11.5	30.0		

1198.50  
1199.84

102+20.1

5.3 1193.2  
~~1194.6~~

102+20.9

5.3 1193.2  
~~1194.6~~

103

5.0 1193.5  
~~1194.9~~

104

2.3 1196.2  
~~1197.6~~

T.P

4.54

1201.68  
1203.04

1.36 1197.14  
~~1198.50~~

105

4.4 1197.3  
~~1198.6~~

106

5.2 1196.5  
~~1197.8~~

107

5.9 1195.8  
~~1197.1~~

107+48.7

6.4 1195.3  
~~1196.6~~

108

6.1 1195.6  
~~1196.9~~

109

5.3 1196.4  
~~1197.7~~

110

5.7 1196.8  
~~1197.3~~

111

7.8 1193.9  
~~1195.2~~

111+86.1

8.4 1193.3  
~~1194.6~~

7.0 6.0 6.9 5.4 5.3 6.0 7.8 8.8 7.0 6.9  
 30.0 20.0 17.5 13.0 12.0 6.6 12.5 13.0 14.5 30.0

1192.4 1192.8 1192.9 1190.1 1190.6 1192.8 1196.2 1191.7 1194.6 1194.6 1195.2 1192.2 1191.0 1195.1

120 111 103 98 93.1 97 5.2 5.3 5.3 4.7 7.2 8.9 6.8  
 30.0 20.0 16.0 50.0 18.1 12.0 3.0 8.7 50.0

7.8 5.6 6.3 5.5 5.0 5.3 4.5 3.6 3.5 3.2  
 30.0 20.0 12.0 14.0 14.0 6.0 8.0 18.0 20.0 30.0

3.2 3.2 3.5 4.8 3.6 2.8 2.3 2.0 3.2 1.8 0.5  
 30.0 25.0 23.0 20.0 16.5 12.0 9.0 5.0 6.0 9.0 30.0

5.3 5.7 4.9 6.0 5.1 4.7 4.6 5.1 4.1 3.1  
 30.0 25.0 22.0 18.0 15.0 13.0 5.0 9.0 16.0 30.0

5.7 5.8 5.7 6.7 5.8 5.2 5.3 5.9 4.9 3.8  
 30.0 23.0 17.0 15.0 11.0 7.0 9.0 13.0 30.0

7.7 7.2 6.5 7.0 6.2 5.9 5.9 6.9 6.2 4.8  
 30.0 20.0 16.5 15.5 11.0 7.0 5.0 9.0 30.0

1192.1 1192.5 1194.5 1192.2 1196.6 1192.4 1195.7 1192.2 1190.9

12.9 9.5 8.5 6.8 6.7 6.6 7.3 5.8 7.1  
 100.0 30.0 12.4 3.0 7.0 8.0 50.0

3.0 3.8 5.5 6.5 6.1 5.8 6.7 6.7 7.1 7.1  
 30.0 25.0 8.0 5.0 2.0 7.0 7.0 23.0 30.0

6.0 5.7 6.1 5.3 5.6 4.7 3.7  
 30.0 15.5 14.5 7.0 6.0 30.0

5.6 5.5 7.1 5.6 5.7 6.0 6.6 5.1 3.7  
 30.0 19.5 17.0 2.0 2.0 4.5 9.0 30.0

1191.4 1194.9 1192.5 1195.2 1195.0 1196.0 1197.1

8.6 8.1 8.5 7.8 8.0 7.0 5.9  
 30.0 20.0 17.0 4.0 8.0 30.0

9.9 9.4 8.3 10.3 8.8 8.4 7.9 9.5 6.3 5.8  
 30.0 20.0 16.0 11.0 7.0 7.9 12.0 30.0

		1201.68		
		<del>1203.14</del>		
		1196.63		
T.P	3.98	<del>1199.99</del>	9.03	1192.166
				<del>1194.01</del>
				1192.9
112			3.7	<del>1194.3</del>
				1195.160
B.M			0.93	<del>1199.86</del>
				1191.0
113			5.6	<del>1192.4</del>
				1189.2
114			7.4	<del>1196.6</del>
				1189.00
T.P	7.63	<del>1199.36</del>		

114

+	+	+	-	-		+	+	+	+
4.7	4.7	3.7	5.7	7.2	3.7	3.2	2.2	2.2	1.7
30.0	25.0	15.0	13.0	10.0	8.5	7.0	7.0	7.0	30.0

W. root 12" Maple 25' Pt. Sta. 112+80

6.4	5.8	7.5	6.2	5.6	5.8	6.6	4.5	3.1	
30.0	12.0	11.0	8.5	6.5	5.0	7.0	12.0	30.0	

7.5	7.9	9.2	7.8	7.7	7.7	9.0	5.8	4.9	
30.0	13.0	11.0	8.5	7.0	5.5	7.5	14.0	30.0	

Top of side stake at sta 115

T.P.	B.35	1192.35 <del>1193.71</del>		1189.00 <del>1190.35</del>
115			5.1	1187.3 <del>1188.6</del>
116			7.0	1185.4 <del>1186.7</del>
T.P.	5.18	1187.72 <del>1189.08</del>	7.81	1182.54 <del>1183.90</del>
117			4.4	1183.3 <del>1184.7</del>
118			6.0	1181.7 <del>1183.1</del>
T.P.	2.96	1184.23 <del>1185.59</del>	6.45	1181.27 <del>1182.63</del>
118+52.9			3.2	1181.0 <del>1182.7</del>
119			4.9	1179.3 <del>1180.7</del>
120			7.4	1176.8 <del>1178.2</del>
121			10.7	1173.5 <del>1174.9</del>
T.P.	2.41	1175.50 <del>1176.86</del>	11.14	1173.09 <del>1174.45</del>
122			5.6	1169.9 <del>1171.3</del>
123			8.8	1166.7 <del>1168.1</del>
124			11.4	1164.1 <del>1165.5</del>
T.P.	6.00	1168.99 <del>1170.35</del>	12.51	1162.99 <del>1164.35</del>
B.M			5.34	1163.65 <del>1165.01</del>

Sun Hot D. Parks 45  
R. Goodrich  
F. Grau

July 8, 1929 70°

Top of side stake sta. 115

4.4	4.9	6.9	5.7	5.1	7.0	4.3	3.4
30.0	12.0	11.0-8.0	7.0	2.0	7.0-8.0	11.0	30.0
5.8	6.5	9.0	7.5	7.0	7.0	8.7	7.5
30.0	15.0	12.0-10.0	9.0	7.0	7.0	10.0	12.0
15.2	4.7	5.3	6.0	7.9	4.4	4.9	6.0
30.0	19.5	15.0	10.0	8.5-6.5	5.0	7.0	9.0-10.0
5.7	6.6	7.5	6.6	6.0	6.2	7.2	6.5
30.0	3.0	7.5	5.0	7.0	7.5	8.5	10.5
17.0	17.0	17.0	17.0	17.0	17.0	17.0	17.0
9.3	8.9	6.8	6.5	4.6-2.0	3.0	3.4	3.2
15.0	10.0	25.0	12.15	10.5	7.5	7.9	11.75
6.5	5.2	5.9	5.3	4.8	5.2	6.4	5.2
30.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0
6.7	6.4	7.2	8.4	7.8	7.4	7.8	9.3
30.0	13.0	9.0	7.5	5.0	7.0	7.0	7.0
9.5	9.8	11.9	10.9	10.7	10.4	10.7	13.1
30.0	7.0	5.0	3.0	7.0	3.0	8.0	12.0
3.1	4.3	7.0	6.0	5.6	5.4	5.9	7.6
30.0	7.0	6.0-5.0	3.0	7.0	7.0	9.5	11.5-13.5
6.8	6.7	8.3	10.0	9.0	8.8	8.8	9.7
30.0	7.0	9.0	6.0-5.0	2.0	7.0	7.0	7.0
10.4	10.6	11.3	12.0	11.5	11.4	11.3	10.5
30.0	18.5	17.5	8.0	4.0	7.0	7.0	7.0

E. root 18" Maple 46' Lt Sta 124+68

125

1168.99  
~~1170.35~~

5.7

1163.3  
~~1164.7~~

125712.65

7.4

1161.4  
~~1162.8~~

<del>1169.9</del>	<del>1171.8</del>	<del>1168.5</del>	<del>1166.4</del>	<del>1164.3</del>	<del>1162.2</del>	<del>1160.1</del>	<del>1158.0</del>	<del>1155.9</del>	<del>1153.8</del>	<del>1151.7</del>	<del>1149.6</del>	<del>1147.5</del>	<del>1145.4</del>	<del>1143.3</del>	<del>1141.2</del>	<del>1139.1</del>	<del>1137.0</del>	<del>1134.9</del>	<del>1132.8</del>	<del>1130.7</del>	<del>1128.6</del>	<del>1126.5</del>	<del>1124.4</del>	<del>1122.3</del>	<del>1120.2</del>	<del>1118.1</del>	<del>1116.0</del>	<del>1113.9</del>	<del>1111.8</del>	<del>1109.7</del>	<del>1107.6</del>	<del>1105.5</del>	<del>1103.4</del>	<del>1101.3</del>	<del>1099.2</del>	<del>1097.1</del>	<del>1095.0</del>	<del>1092.9</del>	<del>1090.8</del>	<del>1088.7</del>	<del>1086.6</del>	<del>1084.5</del>	<del>1082.4</del>	<del>1080.3</del>	<del>1078.2</del>	<del>1076.1</del>	<del>1074.0</del>	<del>1071.9</del>	<del>1069.8</del>	<del>1067.7</del>	<del>1065.6</del>	<del>1063.5</del>	<del>1061.4</del>	<del>1059.3</del>	<del>1057.2</del>	<del>1055.1</del>	<del>1053.0</del>	<del>1050.9</del>	<del>1048.8</del>	<del>1046.7</del>	<del>1044.6</del>	<del>1042.5</del>	<del>1040.4</del>	<del>1038.3</del>	<del>1036.2</del>	<del>1034.1</del>	<del>1032.0</del>	<del>1029.9</del>	<del>1027.8</del>	<del>1025.7</del>	<del>1023.6</del>	<del>1021.5</del>	<del>1019.4</del>	<del>1017.3</del>	<del>1015.2</del>	<del>1013.1</del>	<del>1011.0</del>	<del>1008.9</del>	<del>1006.8</del>	<del>1004.7</del>	<del>1002.6</del>	<del>1000.5</del>	<del>998.4</del>	<del>996.3</del>	<del>994.2</del>	<del>992.1</del>	<del>990.0</del>	<del>987.9</del>	<del>985.8</del>	<del>983.7</del>	<del>981.6</del>	<del>979.5</del>	<del>977.4</del>	<del>975.3</del>	<del>973.2</del>	<del>971.1</del>	<del>969.0</del>	<del>966.9</del>	<del>964.8</del>	<del>962.7</del>	<del>960.6</del>	<del>958.5</del>	<del>956.4</del>	<del>954.3</del>	<del>952.2</del>	<del>950.1</del>	<del>948.0</del>	<del>945.9</del>	<del>943.8</del>	<del>941.7</del>	<del>939.6</del>	<del>937.5</del>	<del>935.4</del>	<del>933.3</del>	<del>931.2</del>	<del>929.1</del>	<del>927.0</del>	<del>924.9</del>	<del>922.8</del>	<del>920.7</del>	<del>918.6</del>	<del>916.5</del>	<del>914.4</del>	<del>912.3</del>	<del>910.2</del>	<del>908.1</del>	<del>906.0</del>	<del>903.9</del>	<del>901.8</del>	<del>899.7</del>	<del>897.6</del>	<del>895.5</del>	<del>893.4</del>	<del>891.3</del>	<del>889.2</del>	<del>887.1</del>	<del>885.0</del>	<del>882.9</del>	<del>880.8</del>	<del>878.7</del>	<del>876.6</del>	<del>874.5</del>	<del>872.4</del>	<del>870.3</del>	<del>868.2</del>	<del>866.1</del>	<del>864.0</del>	<del>861.9</del>	<del>859.8</del>	<del>857.7</del>	<del>855.6</del>	<del>853.5</del>	<del>851.4</del>	<del>849.3</del>	<del>847.2</del>	<del>845.1</del>	<del>843.0</del>	<del>840.9</del>	<del>838.8</del>	<del>836.7</del>	<del>834.6</del>	<del>832.5</del>	<del>830.4</del>	<del>828.3</del>	<del>826.2</del>	<del>824.1</del>	<del>822.0</del>	<del>819.9</del>	<del>817.8</del>	<del>815.7</del>	<del>813.6</del>	<del>811.5</del>	<del>809.4</del>	<del>807.3</del>	<del>805.2</del>	<del>803.1</del>	<del>801.0</del>	<del>798.9</del>	<del>796.8</del>	<del>794.7</del>	<del>792.6</del>	<del>790.5</del>	<del>788.4</del>	<del>786.3</del>	<del>784.2</del>	<del>782.1</del>	<del>780.0</del>	<del>777.9</del>	<del>775.8</del>	<del>773.7</del>	<del>771.6</del>	<del>769.5</del>	<del>767.4</del>	<del>765.3</del>	<del>763.2</del>	<del>761.1</del>	<del>759.0</del>	<del>756.9</del>	<del>754.8</del>	<del>752.7</del>	<del>750.6</del>	<del>748.5</del>	<del>746.4</del>	<del>744.3</del>	<del>742.2</del>	<del>740.1</del>	<del>738.0</del>	<del>735.9</del>	<del>733.8</del>	<del>731.7</del>	<del>729.6</del>	<del>727.5</del>	<del>725.4</del>	<del>723.3</del>	<del>721.2</del>	<del>719.1</del>	<del>717.0</del>	<del>714.9</del>	<del>712.8</del>	<del>710.7</del>	<del>708.6</del>	<del>706.5</del>	<del>704.4</del>	<del>702.3</del>	<del>700.2</del>	<del>698.1</del>	<del>696.0</del>	<del>693.9</del>	<del>691.8</del>	<del>689.7</del>	<del>687.6</del>	<del>685.5</del>	<del>683.4</del>	<del>681.3</del>	<del>679.2</del>	<del>677.1</del>	<del>675.0</del>	<del>672.9</del>	<del>670.8</del>	<del>668.7</del>	<del>666.6</del>	<del>664.5</del>	<del>662.4</del>	<del>660.3</del>	<del>658.2</del>	<del>656.1</del>	<del>654.0</del>	<del>651.9</del>	<del>649.8</del>	<del>647.7</del>	<del>645.6</del>	<del>643.5</del>	<del>641.4</del>	<del>639.3</del>	<del>637.2</del>	<del>635.1</del>	<del>633.0</del>	<del>630.9</del>	<del>628.8</del>	<del>626.7</del>	<del>624.6</del>	<del>622.5</del>	<del>620.4</del>	<del>618.3</del>	<del>616.2</del>	<del>614.1</del>	<del>612.0</del>	<del>609.9</del>	<del>607.8</del>	<del>605.7</del>	<del>603.6</del>	<del>601.5</del>	<del>599.4</del>	<del>597.3</del>	<del>595.2</del>	<del>593.1</del>	<del>591.0</del>	<del>588.9</del>	<del>586.8</del>	<del>584.7</del>	<del>582.6</del>	<del>580.5</del>	<del>578.4</del>	<del>576.3</del>	<del>574.2</del>	<del>572.1</del>	<del>570.0</del>	<del>567.9</del>	<del>565.8</del>	<del>563.7</del>	<del>561.6</del>	<del>559.5</del>	<del>557.4</del>	<del>555.3</del>	<del>553.2</del>	<del>551.1</del>	<del>549.0</del>	<del>546.9</del>	<del>544.8</del>	<del>542.7</del>	<del>540.6</del>	<del>538.5</del>	<del>536.4</del>	<del>534.3</del>	<del>532.2</del>	<del>530.1</del>	<del>528.0</del>	<del>525.9</del>	<del>523.8</del>	<del>521.7</del>	<del>519.6</del>	<del>517.5</del>	<del>515.4</del>	<del>513.3</del>	<del>511.2</del>	<del>509.1</del>	<del>507.0</del>	<del>504.9</del>	<del>502.8</del>	<del>500.7</del>	<del>498.6</del>	<del>496.5</del>	<del>494.4</del>	<del>492.3</del>	<del>490.2</del>	<del>488.1</del>	<del>486.0</del>	<del>483.9</del>	<del>481.8</del>	<del>479.7</del>	<del>477.6</del>	<del>475.5</del>	<del>473.4</del>	<del>471.3</del>	<del>469.2</del>	<del>467.1</del>	<del>465.0</del>	<del>462.9</del>	<del>460.8</del>	<del>458.7</del>	<del>456.6</del>	<del>454.5</del>	<del>452.4</del>	<del>450.3</del>	<del>448.2</del>	<del>446.1</del>	<del>444.0</del>	<del>441.9</del>	<del>439.8</del>	<del>437.7</del>	<del>435.6</del>	<del>433.5</del>	<del>431.4</del>	<del>429.3</del>	<del>427.2</del>	<del>425.1</del>	<del>423.0</del>	<del>420.9</del>	<del>418.8</del>	<del>416.7</del>	<del>414.6</del>	<del>412.5</del>	<del>410.4</del>	<del>408.3</del>	<del>406.2</del>	<del>404.1</del>	<del>402.0</del>	<del>399.9</del>	<del>397.8</del>	<del>395.7</del>	<del>393.6</del>	<del>391.5</del>	<del>389.4</del>	<del>387.3</del>	<del>385.2</del>	<del>383.1</del>	<del>381.0</del>	<del>378.9</del>	<del>376.8</del>	<del>374.7</del>	<del>372.6</del>	<del>370.5</del>	<del>368.4</del>	<del>366.3</del>	<del>364.2</del>	<del>362.1</del>	<del>360.0</del>	<del>357.9</del>	<del>355.8</del>	<del>353.7</del>	<del>351.6</del>	<del>349.5</del>	<del>347.4</del>	<del>345.3</del>	<del>343.2</del>	<del>341.1</del>	<del>339.0</del>	<del>336.9</del>	<del>334.8</del>	<del>332.7</del>	<del>330.6</del>	<del>328.5</del>	<del>326.4</del>	<del>324.3</del>	<del>322.2</del>	<del>320.1</del>	<del>318.0</del>	<del>315.9</del>	<del>313.8</del>	<del>311.7</del>	<del>309.6</del>	<del>307.5</del>	<del>305.4</del>	<del>303.3</del>	<del>301.2</del>	<del>299.1</del>	<del>297.0</del>	<del>294.9</del>	<del>292.8</del>	<del>290.7</del>	<del>288.6</del>	<del>286.5</del>	<del>284.4</del>	<del>282.3</del>	<del>280.2</del>	<del>278.1</del>	<del>276.0</del>	<del>273.9</del>	<del>271.8</del>	<del>269.7</del>	<del>267.6</del>	<del>265.5</del>	<del>263.4</del>	<del>261.3</del>	<del>259.2</del>	<del>257.1</del>	<del>255.0</del>	<del>252.9</del>	<del>250.8</del>	<del>248.7</del>	<del>246.6</del>	<del>244.5</del>	<del>242.4</del>	<del>240.3</del>	<del>238.2</del>	<del>236.1</del>	<del>234.0</del>	<del>231.9</del>	<del>229.8</del>	<del>227.7</del>	<del>225.6</del>	<del>223.5</del>	<del>221.4</del>	<del>219.3</del>	<del>217.2</del>	<del>215.1</del>	<del>213.0</del>	<del>210.9</del>	<del>208.8</del>	<del>206.7</del>	<del>204.6</del>	<del>202.5</del>	<del>200.4</del>	<del>198.3</del>	<del>196.2</del>	<del>194.1</del>	<del>192.0</del>	<del>189.9</del>	<del>187.8</del>	<del>185.7</del>	<del>183.6</del>	<del>181.5</del>	<del>179.4</del>	<del>177.3</del>	<del>175.2</del>	<del>173.1</del>	<del>171.0</del>	<del>168.9</del>	<del>166.8</del>	<del>164.7</del>	<del>162.6</del>	<del>160.5</del>	<del>158.4</del>	<del>156.3</del>	<del>154.2</del>	<del>152.1</del>	<del>150.0</del>	<del>147.9</del>	<del>145.8</del>	<del>143.7</del>	<del>141.6</del>	<del>139.5</del>	<del>137.4</del>	<del>135.3</del>	<del>133.2</del>	<del>131.1</del>	<del>129.0</del>	<del>126.9</del>	<del>124.8</del>	<del>122.7</del>	<del>120.6</del>	<del>118.5</del>	<del>116.4</del>	<del>114.3</del>	<del>112.2</del>	<del>110.1</del>	<del>108.0</del>	<del>105.9</del>	<del>103.8</del>	<del>101.7</del>	<del>99.6</del>	<del>97.5</del>	<del>95.4</del>	<del>93.3</del>	<del>91.2</del>	<del>89.1</del>	<del>87.0</del>	<del>84.9</del>	<del>82.8</del>	<del>80.7</del>	<del>78.6</del>	<del>76.5</del>	<del>74.4</del>	<del>72.3</del>	<del>70.2</del>	<del>68.1</del>	<del>66.0</del>	<del>63.9</del>	<del>61.8</del>	<del>59.7</del>	<del>57.6</del>	<del>55.5</del>	<del>53.4</del>	<del>51.3</del>	<del>49.2</del>	<del>47.1</del>	<del>45.0</del>	<del>42.9</del>	<del>40.8</del>	<del>38.7</del>	<del>36.6</del>	<del>34.5</del>	<del>32.4</del>	<del>30.3</del>	<del>28.2</del>	<del>26.1</del>	<del>24.0</del>	<del>21.9</del>	<del>19.8</del>	<del>17.7</del>	<del>15.6</del>	<del>13.5</del>	<del>11.4</del>	<del>9.3</del>	<del>7.2</del>	<del>5.1</del>	<del>3.0</del>	<del>0.9</del>
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B.M. 11/11/11

11/11/11

11/11/11

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11/11/11

F. B. ... Maple ... 12-7-11

Culverts  
B.M. 2.98 1167.99 1165.01

1158.90

1160.10

May 16, 1930 D. Parks, F. Ashcraft, C. Rand  
E. root 18" Maple Left sta 124468

9.09 3.59 C 6.50 stake 37' N.W.,  
7.89 1.39 C 6.50 stake 37' S.E.,

B.M	6.87	1171.88		1165.01
124				1166.60
123				1168.60
	11.77	1181.59	2.06	1169.82
122				1171.90
121				1175.40
120				1178.70
T.P.			2.20	1179.39

49

E. root 18" Maple left sta. 124+68

5.28	5.32	$\frac{0.0}{20.0}$	7.07	$\frac{F1.8}{21.0}$
3.28	1.74	$\frac{0.5}{24.0}$	2.90	$\frac{0.4}{21.0}$
9.69	7.40	$\frac{0.8}{23.5}$	7.22	$\frac{0.5}{24.5}$
6.19	5.16	$\frac{0.0}{22.0}$	4.34	$\frac{0.8}{23.5}$
2.89	2.20	$\frac{0.7}{22.0}$	0.83	$\frac{0.1}{25.0}$

Slope hub Lt. sta. 120+00 0.09 lower than Elev. given  
 T.P. is sunk in the ground

T.P.	7.80	1187.19		1179.39
119				1181.40
118				1183.20
T.P.	7.05	1191.87	2.37	1184.82
117				1185.10
116				1187.20
115				1189.20
T.P.	8.84	1198.29	2.42	1189.45
114				1191.00
113				1192.80
B.M			1.11	1197.18
	1.11	1197.06		1197.06 record

cloudy warm June 17 1930 D. Parks, T. Snyder 50

T.P. Hub has been hit by a tractor 15209 lbs

Slope hub Lt sta. 120+00

5.79	6.82	$\frac{F1.0}{20.0}$	5.86	$\frac{F0.1}{20.0}$
3.99	3.88	$\frac{C0.1}{20.0}$	5.10	$\frac{F1.1}{20.5}$
4.77	4.65	$\frac{C2.1}{22.0}$	4.88	$\frac{C1.9}{23.0}$
4.67	3.86	$\frac{C0.8}{22.0}$	3.65	$\frac{C1.0}{23.0}$
2.67	2.42	$\frac{C0.3}{21.0}$	1.68	$\frac{C1.0}{22.0}$
7.29	7.58	$\frac{F0.3}{20.0}$	4.97	$\frac{C2.3}{24.5}$
5.49	6.22	$\frac{F0.7}{20.0}$	3.74	$\frac{C1.8}{23.5}$

W. root 12" Maple Rt. sta. 112+30

	2.08	1199.14		1197.06
113				1192.80
114				1191.00
115				1189.20
116				1187.20
117	3.58	1190.46	12.26	1186.88
117				1185.10
118				1183.20
119				1181.40
120				1178.70
111+35	2.65	1199.71		1197.06
		pipe culvert		
112				1194.60
111				1196.20
	4.46	1202.48	1.69	1198.02
110				1197.80
109				1198.30
108				1197.80
107+44.7				
		pipe culvert		
107				1197.40
106				1198.10
	4.71	1202.92	4.27	1198.21
105				1198.80

Cloudy, Warm June 17, 1930 D. Forks, T. Snyder 51  
rain from 12:45 till 2:00

W. root 12" Maple		Pt. Sta 112+30	
4.34	7.19	$\frac{F0.9}{20.0}$	4.71 $\frac{C1.6}{23.5}$
8.14	8.56	$\frac{F1.4}{20.0}$	5.96 $\frac{C2.2}{24.5}$
9.94	9.82	$\frac{C0.1}{21.0}$	9.07 $\frac{C0.9}{22.0}$
11.94	11.26	$\frac{C0.7}{22.0}$	11.04 $\frac{C0.9}{23.0}$
		$\frac{C2.0}{22.0}$	
5.36	3.35	$\frac{C2.0}{22.0}$	3.58 $\frac{C1.8}{23.0}$
7.26	7.23	$\frac{0.0}{20.0}$	8.48 $\frac{F1.2}{20.5}$
9.06	10.18	$\frac{F1.1}{20.0}$	9.22 $\frac{F0.2}{20.0}$
11.76	11.15	$\frac{C0.6}{22.0}$	9.66 $\frac{C2.1}{25.0}$
Stake 30' Lt		Stake 30' Rt	
1192.53	7.18	.518	$\frac{C2.0}{23.0}$
			1193.34 6.35 2.35 $\frac{C4.0}{25.0}$
5.11	6.20	$\frac{F1.1}{21.0}$	3.29 $\frac{C1.8}{23.0}$
3.57	4.77	$\frac{F1.3}{18.0}$	2.69 $\frac{C0.8}{22.0}$
4.68	5.64	$\frac{F1.0}{18.5}$	3.20 $\frac{C1.5}{23.0}$
4.18	5.12	$\frac{F0.9}{18.0}$	3.02 $\frac{C1.2}{22.0}$
4.68	6.37	$\frac{F1.7}{23.0}$	3.92 $\frac{C0.8}{18.0}$
Stake 30' Lt		Stake 30' Rt	
1193.88	8.60	6.10	$\frac{C2.6''}{25.0}$
			1194.63 7.85 2.85 $\frac{C5.0}{25.0}$
5.08	4.36	$\frac{F1.3}{20.0}$	4.64 $\frac{C0.4}{21.0}$
4.38	4.64	$\frac{F0.3}{20.5}$	3.72 $\frac{C0.7}{22.0}$
4.12	4.78	$\frac{F0.7}{19.5}$	3.47 $\frac{C0.7}{22.0}$

1202.92

T.P. 3.47 1199.45

T.P. 2.47 1201.92 1199.45

104 1197.80

103 1195.60

102 1195.60

101 1197.70

T.P. 8.54 1208.96 1.50 1200.42

100 1199.80

99 1201.90

98 1203.50

97 1203.00

96 1202.00

95 1201.50

3.91 1206.01 6.86 1202.10

B.M. 1.90 1204.11

94 1.90 1205.93 1204.03

94 1202.50

8.21 1211.26 2.88 1203.05

93 1204.50

92 1206.50

91 1207.50

90+50 1208.00

5.54 1213.58 3.22 1208.04

slope hub 22.0' Ft. Sta. 105700

Cloudy Warm Showers  
June, 18, 1930 D. Parks, T. Snyder

slope hub 22.0' Ft. Sta. 105700

4.12	6.34	<u>F2.2</u> 17.5	2.84	<u>C1.3</u> 23.0
6.32	8.13	<u>F1.8</u> 18.5	5.64	<u>C0.7</u> 23.0
6.32	8.44	<u>F2.1</u> 19.0	9.85	<u>F3.5</u> 21.5
4.22	3.85	<u>C0.4</u> 21.5	3.52	<u>C0.7</u> 22.0
9.16	7.14	<u>C2.0</u> 23.0	8.54	<u>C0.6</u> 23.0
7.06	6.20	<u>C0.9</u> 22.0	6.59	<u>C0.6</u> 21.5
5.46	4.18	<u>C1.3</u> 23.0	1.99	<u>C3.5</u> 26.5
5.96	4.99	<u>C1.0</u> 22.0	4.21	<u>C1.8</u> 23.0
6.96	7.73	<u>F0.8</u> 20.0	6.63	<u>C0.3</u> 21.0
7.46	9.20	<u>F1.7</u> 18.0	8.26	<u>F0.8</u> 20.0

3.43 4.39 F1.0  
19.0 3.53 F0.1  
21.0

6.76	5.87	<u>C0.9</u> 22.0	4.22	<u>C2.5</u> 24.0
4.76	5.31	<u>F0.5</u> 20.5	3.99	<u>C0.8</u> 22.5
3.76	4.05	<u>F0.3</u> 20.5	2.60	<u>C1.2</u> 22.0
3.26	3.83	<u>F0.6</u> 19.5	1.97	<u>C1.3</u> 23.0

90

T.P.

1213.58

1208.50

2.89 1210.67

5.08 5.79  $\frac{F0.7}{22.0}$

4.60  $\frac{60.5}{22.0}$

R.P. spike E. side 18" Maple

	3.06	1213.75		1210.69
89+50				1208.70
89				1208.50
88				1207.50
87				1206.50
	4.19	1209.52	8.42	1205.35
86				1205.50
85				1206.50
T. P.	11.90	1211.20	0.22	1209.30
B.M.			6.24	1204.96
	4.24	1211.11		1204.87 record
T. P.	11.66	1220.87	1.90	1209.21
84				1209.00
83				1213.50
	7.71	1226.50	2.06	1218.81
82				1218.00
81				1222.00
80+50				1223.00
	2.34	1226.89	1.95	1224.55
80				1222.00
79+50				1220.30
77	0.28	1220.93	6.24	1220.65
79				1218.40
78				1216.50
	8.52	1227.98	1.47	1219.46

S.P. E side 18" Maple

	5.05	4.41	$\frac{C0.6}{21.0}$	4.53	$\frac{C0.5}{21.0}$
	<del>5.25</del>	5.47	$\frac{F0.2}{21.0}$	4.28	$\frac{C1.0}{23.0}$
	6.25	5.92	$\frac{C0.3}{21.5}$	5.85	$\frac{C0.4}{20.0}$
	7.25	8.95	$\frac{F1.7}{20.0}$	7.96	$\frac{F0.7}{20.0}$
			$\frac{C1.2}{23.0}$	4.71	$\frac{F0.7}{20.0}$
	3.02	4.72	$\frac{F4.7}{20.0}$	5.35	$\frac{F2.3}{19.0}$

B.M. F. root 24" Catalpa Pt. sta. 84+70

	11.87	10.85	$\frac{C1.0}{22.0}$	12.93	$\frac{F1.0}{20.0}$
	7.37	3.73	$\frac{C3.6}{28.0}$	5.45	$\frac{C1.9}{27.0}$
	8.50	6.03	$\frac{C2.5}{25.0}$	7.19	$\frac{C1.3}{23.0}$
	4.50	3.79	$\frac{C0.7}{22.5}$	3.95	$\frac{C0.6}{22.5}$
	3.50	3.69	$\frac{F0.2}{21.0}$	2.99	$\frac{C0.5}{22.0}$
	4.89	3.89	$\frac{C1.0}{23.0}$	2.34	$\frac{C2.6}{25.0}$
	6.59	5.92	$\frac{C0.7}{23.0}$	3.27	$\frac{C3.3}{26.0}$
			$\frac{F0.7}{24.0}$	0.28	$\frac{C2.3}{24.0}$
	2.53	3.22	$\frac{C0.7}{23.0}$	8.57	$\frac{F4.1}{24.0}$
	4.43	8.13	$\frac{F3.7}{23.5}$		

	SS	H.I.	F.S	Elev	Grade Elev
		1227.98			
77				1217.50	
76				1221.30	
	11.11	1237.45	1.64	1226.34	
75				1227.30	
74				1233.30	
	5.49	1242.38	0.56	1236.89	
B.M.			5.43	1236.95	
	5.43	<del>1242.37</del>		<del>1236.96</del>	revised
73		1241.03		1235.60	Corrected
72				1234.50	
71				1230.00	
73			5.2	<del>1237.2</del>	
72			4.9	<del>1237.5</del>	
71			9.5	1232.9	
	1.34	1229.76		1228.42	
		<del>1231.12</del>	12.61	1229.78	
70			6.5	<del>1229.7</del>	1224.
69			9.8	1221.4	1220.30
68+30			8.7	<del>1222.5</del>	122
68			8.4	<del>1222.8</del>	12203 0
67			6.2	1225.0	1224.30
	12.02	1240.57		1228.55	
		<del>1241.93</del>	1.21	1229.91	
66	0.01	1241.93	8.7	<del>1233.2</del>	1230.30
65			2.6	<del>1239.3</del>	1236.00
	7.05	1247.23	0.39	1240.18	
		<del>1248.59</del>		<del>1241.54</del>	

Grade Rod	Rod	Rod	55
		F1.8	
10.48	12.24	18.0	12.99
		<u>20.5</u>	
6.68	5.03	C1.7	4.52
		<u>22.0</u>	<u>26.0</u>
		C3.6	
10.15	6.58	26.0	5.92
		<u>28.0</u>	
4.15	2.31	C1.8	0.56
		<u>23.0</u>	<u>26.5</u>
E. Root 24" pine Left sta 73+15			
Elevation		C0.2	
5.79	5.29	22.0	2.21
		<u>21.0</u>	<u>26.0</u>
7.89	4.77	C3.1	3.60
		<u>21.0</u>	<u>22.5</u>
12.39	8.47	C3.9	3.94
		<u>23.0</u>	<u>26.5</u>
		C1.6	
11.14	4.1	30.0	8.96
		<u>31.0</u>	<u>34.0</u>
		C1.1	
10.24	8.00	25.0	8.26
		<u>24.0</u>	<u>24.0</u>

1247.23  
~~1248.57~~

B.M.

5.6

1243.0

1243.12

~~1244.48~~

4.11

1241.48 records

4.81 1246.24

64

1240.10

63

1242.50

62

1.90

1244.74

R.P. spike S.W. side 24" Hemlock Pt, 6+13

1243.12 Corrected elevation

6.14 5.06  $\frac{C. 1.1}{21.5}$  6.65  $\frac{F0.5}{20.0}$

3.94 4.75  $\frac{F. 1.0}{20.5}$

1.50 1.90  $\frac{F. 0.4}{18.5}$  0.00  $\frac{C. 1.5}{24.0}$

72

71

70 9.69 1232.06 1224.00

0.20 1222.37

69 9.69 1226.06 1220.30

0.20 1221.24

68 9.54 1222.57 1220.30

12.70 1221.03

+ 67.88 5.34 1233.73 13.05 1228.39 1224.72

66 0.01 1241.49 1230.30

65 B.M. 4.81 1246.24 1241.43 record

64

66 0.01 1241.49 1241.43 record

65 4.81 1246.24 1241.43 record

8.06 8.43  $\frac{F0.4}{17.0}$  2.85  $\frac{C5.2}{28.5}$

2.27 5.82  $\frac{F3.6}{21.0}$  1.81  $\frac{F2.6}{21.0}$

2.27 4.25  $\frac{F2.0}{20.0}$  3.49  $\frac{F1.2}{18.0}$

9.43 8.61  $\frac{C0.8}{22.0}$  10.85  $\frac{F1.4}{12.5}$

9.01 10.86  $\frac{C1.72}{31.0}$  10.50  $\frac{F1.5}{19.5}$

11.14 4.40  $\frac{C6.1}{30.0}$  8.96  $\frac{C2.2}{24.0}$

10.24 8.00  $\frac{C2.2}{25.0}$  8.36  $\frac{C1.9}{24.0}$

Notes run from Bottom up,

11.14 4.40  $\frac{C6.1}{30.0}$  8.96  $\frac{C2.2}{24.0}$   
10.24 8.00  $\frac{C2.2}{25.0}$  8.36  $\frac{C1.9}{24.0}$

BM	0.32	1319.75		1319.43
1				1314.95
2				1312.70
T.P.		8.34		1311.41
3	1.62	1313.03		1309.70
4				1307.10
5				1305.10
6				1303.50
T.P.		9.96		1303.07
7	1.81	1304.88		1301.90
8				1300.30
9				1298.55
10				1295.95
		10.54		1294.34
11	1.97	1296.31		1293.55
BM		1.81		1294.50
12				1293.45

4.80	3.26	$\frac{C15}{23.0}$	9.32	$\frac{C1.5}{23.0}$
7.25	5.86	$\frac{C14}{23.0}$	6.39	$\frac{C0.9}{22.0}$
3.33	1.08	$\frac{C22}{23.5}$	1.54	$\frac{C1.8}{22.5}$
5.93	6.62	$\frac{F0.7}{21.0}$	6.01	$\frac{F0.1}{20.5}$
7.93	8.60	$\frac{F0.7}{20.0}$	9.23	$\frac{F1.3}{19.5}$
9.53	8.67	$\frac{C0.9}{22.0}$	9.62	$\frac{F0.1}{21.0}$
2.98	0.88	$\frac{C2.1}{24.0}$	2.42	$\frac{C0.6}{21.5}$
4.58	3.36	$\frac{C1.2}{22.5}$	2.68	$\frac{C1.9}{23.5}$
6.33	5.35	$\frac{C1.0}{22.5}$	4.21	$\frac{C2.1}{23.5}$
8.93	8.33	$\frac{C0.6}{19.5}$	5.33	$\frac{C3.6}{26.0}$
2.76	4.28	$\frac{F1.5}{20.0}$	3.23	$\frac{F0.5}{20.0}$
2.86	4.88	$\frac{F2.0}{19.5}$	5.24	$\frac{F2.4}{19.5}$

BM	7.09	1301.54		1294.45	- record					
13				1295.20		6.34	2.93	$\frac{C 3.4}{26.5}$	8.09	$\frac{F 1.6}{24.0}$
14				1297.20		4.34	0.65	$\frac{C 3.7}{27.5}$	2.73	$\frac{C 1.6}{24.0}$
15				1299.20		2.34	2.31	$\frac{C 0.2}{21.5}$	2.69	$\frac{F 0.3}{20.5}$
T.P.	2.02	1302.78	0.78	1300.76						
16				1299.20		3.58	1.77	$\frac{C 1.8}{24.5}$	2.73	$\frac{C 0.9}{22.5}$
17				1297.20		5.58	2.78	$\frac{C 2.8}{21.0}$	6.51	$\frac{F 0.9}{19.0}$
T.P.	8.63	1303.57	7.84	1294.94						
18				1295.45		8.12	9.02	$\frac{F 0.9}{18.5}$	10.12	$\frac{F 2.0}{20.5}$
19				1295.20		8.37	9.61	$\frac{F 1.3}{20.0}$	9.67	$\frac{F 1.3}{20.0}$
20				1296.40		7.17	5.58	$\frac{C 1.6}{24.0}$	4.30	$\frac{C 2.9}{25.5}$
21				1298.80		8.51	6.04	$\frac{C 2.5}{25.0}$	5.77 2.78	$\frac{C 2.0}{24.5}$
22	8.32	1307.31	4.58	1298.99						
BM				1301.00		6.31	5.05	$\frac{C 1.3}{23.5}$	5.81	$\frac{C 0.5}{22.0}$
23			3.72	1303.59	record 1303.69					
				1302.20		5.11	3.95	$\frac{C 1.2}{20.5}$	4.89	$\frac{C 0.3}{19.5}$
B.M.	5.13	1308.82		1303.69	- record	VOID				
24				1302.70		6.12	3.21	$\frac{C 2.9}{22.5}$	4.06	$\frac{C 2.1}{21.5}$

25	1308.82			1300.70	8.12	5.54	$\frac{C26}{23.0}$	4.86	$\frac{C33}{21.0}$
26				1298.40	10.42	9.43	$\frac{C10}{20.5}$	7.08	$\frac{C32}{23.5}$
27				1298.00	10.82	10.04	$\frac{C0.8}{20.0}$	10.62	$\frac{C02}{20.0}$
28				1298.80	10.02	5.00	$\frac{C34}{23.0}$	7.82	$\frac{C2.7}{23.0}$
T.P.	6.52	1306.06	9.28	1299.54					
29				1299.40	6.66	2.95	$\frac{C4.2}{24.5}$	3.90	$\frac{C2.7}{22.0}$
30				1298.90	7.16	5.55	$\frac{C16}{21.0}$	6.30	$\frac{C0.8}{20.5}$
31				1299.20	6.86	5.00	$\frac{C18}{21.5}$	6.14	$\frac{C0.7}{20.5}$
B.M.			5.81	1300.25					
32				1300.00					
33				1300.20					
34				1299.30					
35				1298.00					
36				1297.00					

July 1 1930  
 Showers in forenoon  
 Warm Wind in Afternoon

David R. Parks  
 D. T. Snyder

B. M.	1308.07	4.38	7.5	1303.69
23			5.6	1300.6
24			4.1	1309.1
25			6.4	1301.7
26			8.5	1299.6
27			9.3	1298.8
28			8.8	1299.3
29			6.9	1301.2
T. P.	3.03	1304.31	6.79	1301.28
30			4.6	1299.71
31			4.04	1300.27
	4.04	1302.61		1298.57 record
31				1299.20
30				1298.90
29				1299.40
	8.19	1306.43	4.87	1298.24
28				1298.80
27				1298.00
26				1298.40
25				1300.70
24				1302.70
23				1302.20
22				1301.60

Bent spike E. Root 12" Maple Left. sta 22170

B. M. N.W. Root 18" Maple Right (Record 1298.57) Sta 31987

		C 0.2		F 1.0
3,41	3,24	21.5	4,39	20.5
3,71	3,83	F 0.1	4,52	F 0.8
		21.0		20.5
3,21	0,68	C 2.5	2,12	C 1.1
		24.5		22.0
		C 1.7		C 1.0
7,68	5,89	23.0	6,64	23.0
		F 0.7		F 1.5
8,43	9,32	20.0	9,89	20.0
		F 0.8		C 1.6
8,03	8,78	20.0	6,40	23.5
		C 0.9		C 1.6
5,73	4,84	23.0	4,16	24.0
		C 1.2		C 0.7
3,73	2,57	22.5	3,36	21.5
		F 0.3		F 1.3
4,23	4,65	20.5	5,56	19.5

B, M.	6.01	1304,58		1298,57
32				1300,00
33				1300,20
34				1297,30
35				1298,00
T.P.	7.79	1303,63	8.74	1295,84
36				1297,00
37				1296,10
38				1295,70
	5.77	1305,98	3.62	1300,01
39				1297,80
40				1300,00
41				1301,60
42				1303,00
	4.18	1307,68	2.48	1303,50
43				1303,60
B, M.			3.98	1303,70
	3.98	1307,70		1303,72 record
44				1302,80
45				1301,10
46				1297,70
	2.38	1299,85	10.23	1297,47
47				1294,30
48				1291,90
49				1291,00

N.W. root 18" Maple right sta. 30+98				
4.58	1.91	<u>C2.7</u> 25.5	4.00	<u>C0.6</u> 20.5
4.38	4.08	<u>C0.3</u> 22.0	5.67	<u>F1.3</u> 20.5
5.28	1.33	<u>C4.0</u> 23.5	6.16	<u>F0.9</u> 20.0
6.58	8.34	<u>F1.8</u> 17.0	8.70	<u>F2.1</u> 17.0
		<u>C5.1</u>		<u>F1.6</u>
6.63	1.57	<u>25.5</u>	8.20	<u>20.5</u>
7.53	5.88	<u>C1.7</u> 23.0	10.60	<u>F3.1</u> 20.5
7.93	9.57	<u>F1.7</u> 17.0	11.15	<u>F3.2</u> 20.0
		<u>C1.7</u>		<u>17.0</u>
8.18	6.48	<u>22.0</u>	5.97	<u>C2.2</u> 25.0
5.98	7.77	<u>C1.0</u> 23.0	5.92	<u>C0.1</u> 21.0
4.38	2.76	<u>C1.6</u> 23.5	4.16	<u>C0.2</u> 22.0
2.98	2.20	<u>C0.8</u> 22.5	3.26	<u>F0.3</u> 21.0
		<u>C0.3</u>		<u>F1.1</u>
4.08	3.82	<u>21.0</u>	5.14	<u>20.0</u>
R.P. spike, N.W. side 10" Maple Right 43+20				
4.90	4.39	<u>C0.5</u> 22.0	5.73	<u>F0.8</u> 20.0
6.60	4.33	<u>C2.3</u> 24.5	4.61	<u>C2.0</u> 24.0
10.00	7.71	<u>C2.3</u> 24.0	7.02	<u>C3.0</u> 26.0
		<u>F1.3</u>		<u>C0.3</u>
5.55	6.89	<u>17.0</u>	5.27	<u>21.5</u>
7.95	9.32	<u>F1.4</u> 17.5	10.41	<u>F2.5</u> 20.5
8.85	8.95	<u>F0.1</u> 21.0	9.00	<u>F0.2</u> 24.5

1299.85

4.62 1295.47 9.00 1290.85

50 1289.00

T.P. 9.82 1285.65

0.7

6.47 5.78 22.0

0.3

5.14 23.0

Slope Hub right sta 51

51	0.51	1284.16		1285.65
52				1285.00
53				1280.50
				1275.40
54	0.88	1274.11	12.93	1273.23
55				1270.00
56				1265.30
				1261.80
57	0.25	1261.42	12.94	1261.17
58				1258.40
59				1256.30
60				1253.70
				1251.00
61	0.63	1254.60	7.45	1253.97
62			10.2	1247.80
63			12.3	
	2.92	1245.44	12.88	1242.52
B.M.			3.95	1241.49
				1241.43 record
T.P	1.64	1287.29		1285.65
	0.13	1276.97	10.45	1276.84
	3.05	1269.37	10.65	1266.32
B.M.			9.11	1260.26
				1260.19 record

July 2 1930 D. R. Parks  
cloudy T. Snyder

64

Slope Hub right sta. 51+00

1.16	1.34	$\frac{F0.2}{19.5}$					0.51	$\frac{C0.7}{22.0}$	
5.66	4.38	$\frac{C1.3}{23.5}$					4.50	$\frac{C1.2}{23.0}$	
11.76	11.59	$\frac{F0.8}{20.0}$					6.84	$\frac{C3.9}{26.0}$	
		$\frac{F2.1}{19.5}$						$\frac{C2.4}{24.5}$	
4.11	6.22	$\frac{F2.5}{18.0}$					1.71	$\frac{C1.0}{23.0}$	
8.81	11.32	$\frac{F0.3}{19.0}$					7.79	$\frac{C0.1}{22.0}$	
12.31	12.61	$\frac{F0.3}{21.0}$					12.25	$\frac{F0.2}{24.5}$	
		$\frac{F0.8}{19.0}$						$\frac{C3.4}{25.0}$	
3.02	3.31	$\frac{F0.4}{20.5}$					3.19	$\frac{C2.6}{24.5}$	
5.12	5.94	$\frac{C0.4}{22.0}$					1.68	$\frac{C3.0}{25.0}$	
7.72	8.11	$\frac{F0.5}{20.0}$					5.14	$\frac{C2.9}{24.5}$	
10.42	10.07						7.44		
6.80	7.33						3.91		

S.W. side 24" pine RT, sta. 64+13

Slope Hub right sta 51+00

Spike S.W. side wild Cherry RT, sta. 56+70

# Tile drain

(B.M.)	10.03	1251.46	1241.43
62+50			1241.50
62			1242.70
61+50			1244.25
61			1245.80
60+50			1247.40

S. W. side 24" Pipe Right sta 64+13

9.94	7.58	$\frac{02.38}{20} = 02'4\frac{9}{16}"$
8.74	5.57	$\frac{03.19}{20} = 03'2\frac{1}{4}"$
7.21	2.84	$\frac{04.37}{20} = 04'4\frac{7}{16}"$
5.66	1.74	$\frac{03.92}{20} = 03'11\frac{1}{2}"$
4.06	0.00	$\frac{04.06}{20} = 04'3\frac{3}{4}"$

B.M. 2.77 1242.94 1260.19  
57+75

57+75

T.P. 10.76 1296.41 1285.65  
48+08

B.M. 4.07 1307.79 1303.72

L.M. 3.61 1299.88 11.52 1296.27

37+89

37+89

5.24 1302.67 2.55 1297.33

35+07

66  
S.W. side Wild Cherry Right, sta 56+70

1253.45 9.51 6.51 c3'0" Stake 30' Left

1254.95 8.01 2.51 c5'6" Stake 30' Right

Slope Hub right sta. 57+00

1288.76 7.45 4.45 c3'0" stake 30' Left

1287.29 9.12 6.62 c2'6" stake 30' Right

R.P. spike N.W. side 10" Maple Right 43+20

1292.28 7.60 4.60 c3'0" stake 30' Left

1290.77 9.11 6.11 c3'0" stake 30' Right

1294.20 8.47 4.47 c4'0" stake 30' Left

1292.84 9.83 6.83 c3'0" stake 30' Right

B.M. 5.35 1303.92 1298.57

30+36.4

B.M. 3.94 1302.51 1298.57

27+06

B.M. 0.94 1304.63 1303.69

18+30

N.W. Root 18" Maple Right sta <sup>(30+98)</sup> 31+98

1296.67 7.25 3.25 c4'0" stake 30' left

1295.84 8.08 5.58 c2'6" stake 30' Right

N.W. Root 18" Maple Right sta. <sup>(30+98)</sup> 31+98

1295.48 7.03 4.53 c2'6" stake 30' left

1294.64 7.87 4.87 c3'0" stake 30' Right

Bent spike E. root 12" Maple left sta 22+10

1292.63 12.00 8.00 c4'0" stake 30' left

1291.88 12.75 10.25 c2'6" stake 30' Right

B.M.	4.66	1169.67		1165.01
125				1164.70
124				1164.60
123				1168.60
	9.94	1178.54	1.07	1168.60
122				1171.90
121				1175.40
120	10.53	1184.03	3.04	1175.50
120				1178.70
119				1181.40
	10.34	1192.82	3.55	1182.48
118				1183.20
117				1185.10
116				1187.20
115				1189.20
114				1191.00
	7.80	1198.81	1.81	1191.01
113				1192.80
B.M.			1.74	1197.07
	1.74	1198.80		1197.06 record
112				1197.60
111				1196.20
110				1197.80
T.P.			1.00	1197.80

Finish Grade

E. root 18" Maple Left, Sta. 124+68

4.97	4.94	0.0
3.07		
1.07		
6.64		
3.14		
7.33		
4.63		
9.62		
7.72		
5.62		
3.62		
1.82		
6.01		

W. root 12" Maple 25' RT sta 112+30

(Plans shows 1199.06) (Book shows 1197.06)

4.20
2.60
1.00

finish grade stake RT, sta 110

July 11, 1930 D. Parks, E. Belding, T. Snyder

Warrr West Wind

T.P	4.98	1202.58		1197.80
109				1198.30
108				1197.80
107				1197.40
	5.45	1202.84	5.39	1197.39
106				1198.10
105				1198.80
104				1197.80
103				1195.60
102				1195.60
101				1197.70
	8.53	1206.20	5.17	1197.67
100				1199.80
99				1201.90
98				1203.60
97				1203.00
B.M			2.15	1204.05
	2.15	1206.18		1204.03 record
96				1202.00
95				1201.50
	6.54	1208.03	4.69	1201.49
94				1204.50
93				1204.50
	8.39	1212.89	3.53	1204.50
92				1206.00

finish Grade stake Rt, sta 110

4.48

4.98

5.38

4.74

4.04

5.04

7.24

7.24

5.14

6.40

4.30

2.70

3.20

W. Root 30" Maple Right sta 96+50

4.18

4.68

5.53

3.53

finish Grade stake Lt, sta, 93

6.39

1212.89

91				
90+50				
90				

1207.50
1208.00
1208.50

1208.00	4.89
1208.50	4.39
1209.00	3.89

1207.00	5.89
1207.50	5.39
1208.00	4.89

3.86 1212.87 3.88 1209.01

89+50				
89				
88				
87				

1208.70
1209.50
1207.50
1206.50

1209.20	3.67
1209.00	3.87
5.37	
6.37	

1208.20	4.67
1208.00	4.87

3.80 1210.30 6.37 1206.50

86				
85				

1205.50
1206.50

4.88
3.80

B.M 5.41 1204.89

1204.87 record

(W) E. root 24" Catalpa Right Sta 84+70

July 12, 1930 D. Parks, T. Snyder, E. Belding  
Fair 80°

B.M.	7.48	1212.35		1204.87
84				1209.00
	8.34	1220.17	0.52	1211.83
83				1213.50
82				1218.00
	8.15	1226.10	2.22	1217.95
81				1222.00
81+50				1223.00
80				1222.00
79+50				1220.30
79				1218.40
	5.85	1223.95	8.00	1218.10
78				1216.50
77				1217.50
76				1221.30
	7.92	1231.68	0.19	1223.76
75				1227.30
	8.36	1239.48	0.56	1231.12
74				1233.30
B.M.			2.55	1236.93
	4.43	1241.39		1236.96 record
73				1236.90

E. root 24" Catalpa Right Sta 84+70  
3.35  
6.67  
2.17

1221.50	4.60	1222.50	3.60
1222.50	3.60	1223.50	2.60
1221.50	4.60	1222.50	3.60
1219.80	6.30	1220.80	5.30
1217.90	8.20	1218.90	7.20

7.45  
6.45  
2.65  
4.38  
6.18

Stake on Rt 1.65 C1.0  
Stake on Rt 1.65 C1.0

E. root 24" Pine Left Sta. 73+15  
Stake on Lt 5.49 F1.0  
4.49

B.M. 1.80 1243.23 1241.43

45 1236.00

1.51 1236.27 8.47 1234.76

64 1230.30

0.47 1228.61 8.13 1228.14

67 1224.30

68 1220.30

69 1220.30

70 1224.00

7.58 1235.61 0.58 1228.03

71 1230.00

72 1234.60

S.W. side 24" pine Pt. sta 64+13

7.23

5.97

4.31

8.31

8.31

4.61

5.61

1.11

3.11 F2.0

2.61 F1.5

B.M. 5.85 1247.28 1241.43  
 64 1240.10  
 63 1242.50  
 62 1244.70  
 12.52 1259.55 0.25 1247.03  
 61 1247.80  
 60 1251.00  
 59 1253.70  
 58 1256.30  
 57 1258.40

9.91 1269.19 0.27 1259.28  
 B.M. 8.97 1260.22  
 8.97 1269.16 1260.19 record  
 56 1261.80  
 55 1265.30  
 12.36 1280.37 1.15 1268.01  
 54 1270.00  
 53 1275.40  
 10.88 1279.50 0.75 1277.62  
 52 1280.50  
 51 1285.00  
 50 1289.00  
 T.P. 9.16 1298.16 1.50 1289.00  
 49 1291.00  
 48 1291.90

S.W. side 24" pine Right sta, 64+13  
 7.18  
 4.78  
 2.58  
 11.75  
 8.55  
 5.85  
 3.25  
 1.15

Spiko, S.W. side Wild Cherry Rt, sta 56+70  
 7.36  
 3.86  
 10.37  
 9.97  
 10.00  
 5.50  
 1.50  
 finish Grade Stake Rt, sta 50  
 7.16  
 6.26

1298.16

47

1294.30

3.86

46

1297.70

0.46

8.83 1306.56 0.43 1297.73

45

1301.10

5.44

44

1302.80

3.76

43

1303.60

2.96

B. M.

2.87 1303.69

R. P. spike, N. W. side 10" Maple Pt., 4312

1303.72 record

B.M	4.37	1308.09		1303.72
42				1303.00
41				1301.60
40				1300.00
39				1297.80
	3.96	1301.79	10.24	1297.83
38				1296.70
37				1296.10
36				1297.00
35				1298.00
34				1299.30
33				1300.20
32				1300.00
I.P.	3.98	1303.98	1.79	1300.00
31				1299.20
B.M			5.38	1298.60
	5.38	1303.95		1298.57 record
30				1298.90
29				1299.40
28				1298.80
27				1298.00
	9.66	1305.76	7.85	1296.10
27				1298.00
26				1298.40
25				1300.70

R.P. spike N.W. side 10" Maple Rt. 43120

	5.09
	6.49
	8.09
	10.29
	6.09
	5.69
	4.79
	3.79
	2.49
	1.59
	1.79
finish Grade stake Rt. sta 32	
	4.78
N.W. root 18" Maple right sta 31+98	
	5.05
	4.55
	5.15
	5.95
	LT
	7.76
	RT
	7.36
	5.06

		1305.76			
24				1302.70	
23				1302.20	
B.M.			3.73	1302.03	
	3.73	1307.42		1303.69	record
22				1301.00	
	2.10	1303.11	6.41	1311.01	
21				1291.80	1298.80
20				1296.40	
19				1296.40	1295.20
18				1295.45	
17				1295.20	1297.20
	5.53	1302.73	5.91	1297.20	
16				1299.20	
15				1299.20	
14				1297.20	
13				1295.20	
12				1293.45	
	7.23	1300.27	9.69	1293.04	
11				1293.55	
10				1295.95	
9				1298.55	
8	9.99	1302.52	1.74	1298.53	
8				1300.30	
7				1301.90	
6	7.27	1310.69	5.10	1303.42	

3.06

3.56

Bent spike E. root 12" Maple Lt. 22+70

6.42

4.31

6.71

7.91

7.66

5.91

3.53

3.53

5.53

7.53

9.28

6.72

4.32

1.72

8.22

6.62

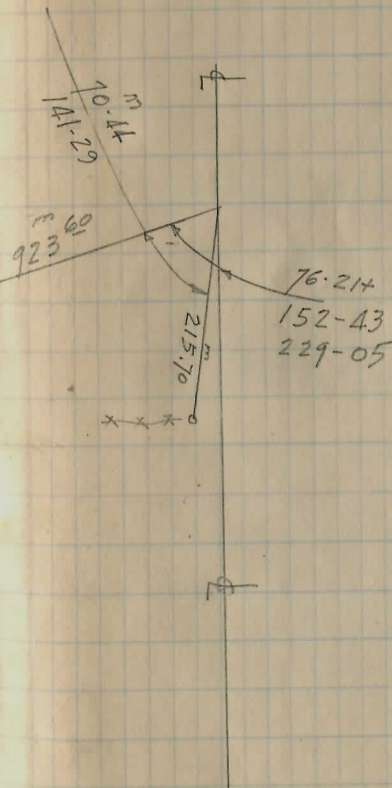
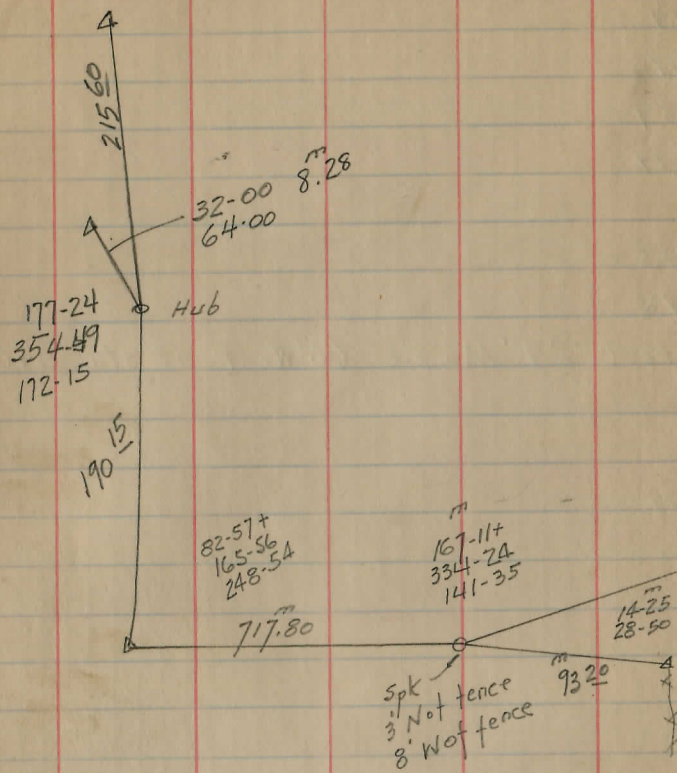
B.M. at 11+02 Has been ruined

1310.69

6				1303.50
5				1305.10
4				1307.10
3				1309.70
	11.43	1321.13	0.99	1309.70
2				1312.70
1				1314.95
B, M		1.67	1319.46	
			1319.43	record

7.19
5.59
3.59
0.99
8.43
6.18

E. root 24" Maple 60' west of sta. 0+00



Brakeman Rd culverts

11475	3x3 stone & conc	28.5'	28.5'
18+30	24" x 40'	Rust East	
27+06	15" x 36'	Rust Ends	
30+36	15" x 36'	Good N.C. cleaned	
35+07	15" x 44'	Rust - East end	
37+89	18" x 40'	Rust - W. End Bant	
48+08	15" x 40'	Rust - needs clean	
57+75	15" x 48'	30° skew	Rustal
78+04	4x4x35	stone & conc	
85+23	<del>3x3</del> 5x35 x 34	stone & conc	
95+19	3x3x33	" "	Stone slipping + 9' W End
102+21	3.5x3x34	- ON	" "
107+45	15" x 40'	- Rusted	
111+35	15" x 36'	- Rusted	
118+53	2'8" x 3' x 30'	Stone & conc	* Full of silt
125+12.65	4' x 3' x 49'6"	conc	Headwall cracked
	45° skew	needs cleaned	EAST END

# EDWARDS SHEET METAL WORKS, INC.

FREDERICKTOWN, OHIO

H. E. BIEFNES

PHONE MYRA 4-5581

W. M. JAMES

**CORRUGATED METAL PIPE**

**WINDOW WELLS**

**STRUCTURAL STEEL BRIDGES**

MEETS STATE AND FEDERAL REGULATIONS

18+30

Not too good

27+06

" " "

30+36

" " "

35+07

OK

37+89

W end rusted  
not too bad

48+08

W end bent in  
E end rusted  
neckt so gut

57+75

Not bad

68+04

3 1/2 x 4 x 21.5

OK

15' or less part 200'  
ea ~~two~~ side

**QUICK DELIVERIES BY TRUCK**

**QUICK DELIVERIES BY TRUCK**

# EDWARDS SHEET METAL WORKS, INC.

FREDERICKTOWN, OHIO

H. E. BIEFNES

PHONE MYRA 4-5581

W. M. JAMES

**CORRUGATED METAL PIPE**

WINDOW WELLS

STRUCTURAL STEEL BRIDGES

MEETS STATE AND FEDERAL REGULATIONS

7840 ✓ OK 16' part

85423 OK

95419 OK 15.5' part

102421 OK 14.5' part

107445 not too good

111435 " " " 15' - part

118453 OK 15' - part

**QUICK DELIVERIES BY TRUCK**

#22  
1955

**WILLIAM R. McGARRY**

1256 Perkinswood Boulevard, S. E.

Warren, Ohio

Telephone: WARREN 36965

11775 3x3x28.5 STONE BOX

SHIRT END EAST LONGER WEST  
NORTH FROZEN STONE SHOVING IN  
CAPSTONE SETTLED. PAVEMENT SHOWS  
WEAKNESS. LOTS MUD CLEAR OUTLET NE

18430 24" COR 1P x 40

BOTTOM WEST END RUSTIER THRU  
SHOULD HAVE BEEN SKEW NW-SE  
CLEAR BOTTOM ROCKS →

27706

15" x 36' COR 1P

RUSTED WEST END - CLEAR →

30436 15" x 36' COR 1P CLEAR

RUSTED BOTH ENDS →

35467 15" x 44' COR 1P CLEAR →

RUSTY SIDES EAST END

**WILLIAM R. McGARRY**

1256 Perkinswood Boulevard, S. E.

Warren, Ohio

Telephone: WARREN 36965

37489 18" x 48' Cor I.P. Bottom Rusted out  
on west end mudded up  $\frac{1}{4}$   $\rightarrow$

48408 15" x 48' Cor I.P. Rusty  $\rightarrow$   
East end undercut. W. end 3' at level -  
Rusty  $\frac{3}{4}$  Alder tree under. Gutter around

57475 15" x 48' S.W. Cor I.P. BE NW Rusty  
Flows NW across road. Natural flow  $\leftarrow$   
obstructed by willows. H<sub>2</sub>O pockets tall  
deep to overflow in along road ditch

68404 Conc slab top on stone walls  
looks ok but too damn short. 4x4x215 D<sub>100</sub>  
H<sub>2</sub>O flows to pavement. Insufficient safety  
Spring Fed Creek deep off road  $\leftarrow$

78404 5' wide x 3x35 Conc top-wall-walk  
OK  $\leftarrow$  where curves in?

815423 #3x3x34 Filthy cess pool. Need  
sanitary engineer first. Probably needs  
rebuilding. Clean outlet flow NW  $\leftarrow$

(JUN 72)

**WILLIAM R. McGARRY**

**1256 Perkinswood Boulevard, S. E.**

**Warren, Ohio**

**Telephone: WARREN 36965**

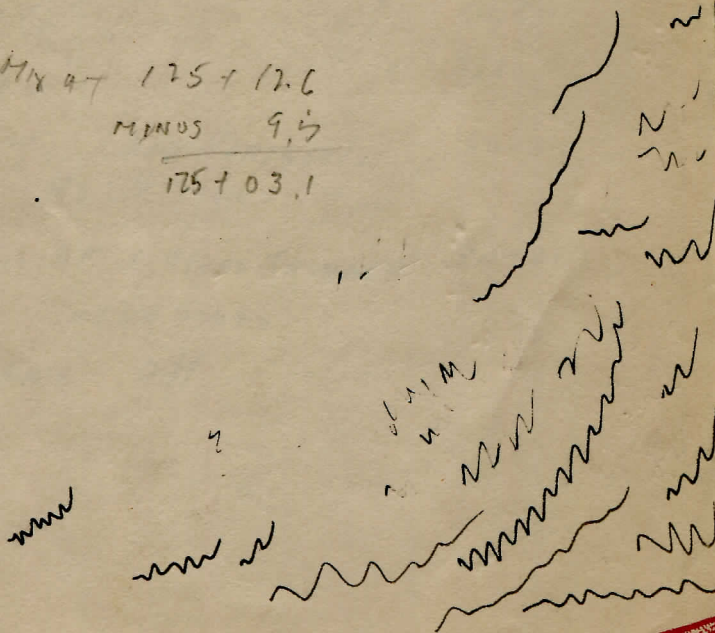
118+53 2.8' WIDE 1.5 FOOT CLEARANCE TO HOOD  
SLABS FALLEN IN NEAR CENTER  
PROBLY SPRING RCD FLOW WEST

125+1265

STAD MIX AT 125+12.6  
MINUS 9.5  

---

125+03.1



TR 475

**WILLIAM R. McGARRY**

**1256 Perkinswood Boulevard, S. E.**

**Warren, Ohio**

**Telephone: WARren 36965**

75 MPH

249' NSPD over POT 15400

270' NSPD over POT 24400

351' " " POT 43

288' " " TOT 49450

396' " " 64450

186' " " 7540

204' (Bad Horizontal) 8040  
NEED SIGNS TOO

Horiz OK if trees TRIMMED 90708!  
NEED SIGNS

ZANANY OK